



Single-Inductor Dual-Output Buck-Boost Power Factor Correction Converter

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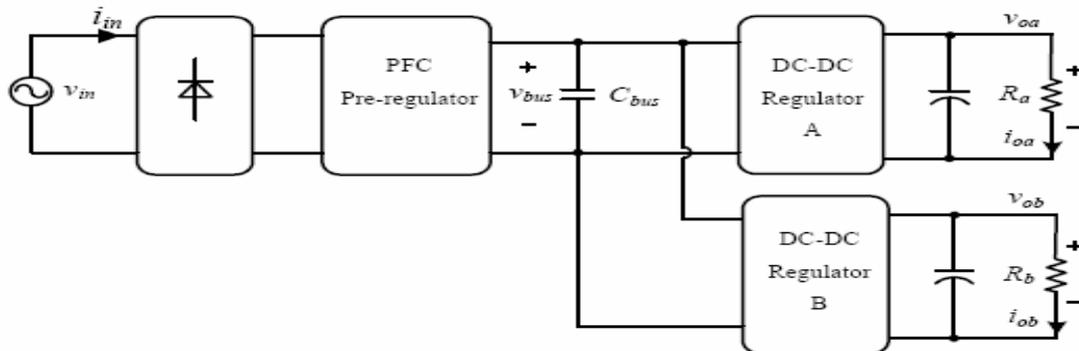
ABSTRACT: In this paper a single-inductor dual-output (SIDO) buck-boost PFC converter operating in critical conduction mode (CRM) is proposed. By multiplexing a single inductor, each output of SIDO buck-boost converter can be regulated independently. Compared with conventional two-stage multiple output converter, SIDO buck-boost PFC converter benefits from significant overall cost saving, small size and light weight. Moreover, the efficiency of SIDO buck-boost PFC converter can be improved due to single-stage power conversion. Control strategy and characteristics of the proposed converter are analyzed. The efficiency, power factor, total harmonic distortion (THD) and output accuracy are verified experimental results.

KEYWORDS: Critical conduction mode (CRM), Power factor correction (PFC), Single stage, Single-inductor dual-output (SIDO), Time multiplexing (TM).

I. INTRODUCTION

Multiple outputs ac/dc power converter has been becoming popular with fast development of consumer electronics and LED lighting[1]-[3], such as multi-level voltage supply system, current balancing for multiple LED string driving, RGB LED lighting, etc. IEC61000-3-2 Class C for lighting equipment establishes a strict requirement for input current harmonic content of power converter [4]. Power factor correction (PFC) is usually used to provide sinusoidal input current. Hence, research of multiple outputs ac/dc power converter with low cost and high power factor is important. In order to achieve high power factor (PF) and to accurately regulate output voltages or currents of multiple output ac/dc converter, conventional multiple output ac/dc power converter consisting of two-stage power conversion is utilized, as shown in Fig.1, where PFC pre-regulator provides dc bus voltage v_{bus} , and parallel connected dc-to-dc regulators are used to regulate output voltage or output current from v_{bus} [5]. The circuit configuration of multiple output ac/dc converter shown in Fig.1 is complex and suffers from high cost, with multiple inductors and controllers are required [6],[7]. Moreover, the two-stage power conversion with PFC pre regulator and dc-to-dc converters suffer from lower efficiency and higher volume and cost. However, single-stage PFC converter can achieve high PF and output current or voltage regulation at the same time [8], [9]. Hence, it has drawn more and more attention in recent years. Flyback PFC converter with multiple secondary windings is a typical single-stage multiple outputs converter, with only one output can be well regulated. Multiple secondary windings in the transformer leads to cross-regulation due to leakage inductance, forward voltage drop of diodes, and series resistance of the windings [10].

Fig.1. Block diagrams of a conventional multiple output ac/dc power converters with high power



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Moreover, only voltage output regulation can be achieved, while multiple current outputs are hard to regulate independently. In order to achieve high accurate regulation of multiple output converter, magnetic amplifier post-regulator approach is applied in [11], [12], but it still requires multiple inductors and windings.

Single-inductor multiple-output (SIMO) converter with only one inductor benefits from significant overall cost saving, small size and light weight, which make it as one of the most suitable and cost-effective solutions for multiple output power supplies. SIMO dc/dc converters in mobile application have been studied in recent years [13]-[17]. In some offline applications, such as LED lighting, single stage PFC converters are preferred. Single-stage buck-boost PFC converter has the advantage of low cost and high power factor, which make it widely applied in single-output non-isolated general lighting application [18]. In this paper, a novel single inductor dual-output (SIDO) buck-boost PFC converter operating in critical conduction mode (CRM) is proposed. Its control strategy and corresponding characteristics are analyzed. Independent regulation of each output can be achieved in this converter by multiplexing a single inductor. Compared with conventional two-stage multiple output converter, the proposed converter benefits with significant overall cost saving, small size, light weight and high power conversion efficiency due to single stage power conversion. The proposed converter can also be easily extended to realize SIMO buck boost PFC converter to fulfil different system requirements. This paper is organized as follows. In Section II, SIDO buck-boost PFC converter is proposed and analyzed. The design considerations and analysis are described in Section III. The experimental results including efficiency, power factor, total harmonic distortion (THD) and output regulation accuracy are given in Section IV, and Section V summarizes the conclusions drawn from the study.

II. PROPOSED SIDO BUCK-BOOST PFC CONVERTER

As shown in Fig.2 (a), the power stage of SIDO buck-boost PFC converter consists of a diode bridge D_{bridge} , an input filter consists of L_f and C_f , three switch networks consists of Q_1 , Q_2 and Q_3 and their corresponding sense resistors R_{s1} , R_{s2} and R_{s3} , two freewheeling diodes D_1 and D_2 , a time-multiplexing inductor L and two output filter capacitors C_1 and C_2 . Q_2 and Q_3 are the time-multiplexing control switches of each output. When Q_2 is turned on and Q_3 is turned off, converter transfer power to output A, and when Q_2 is turned off and Q_3 is turned on, converter transfer power to output B.

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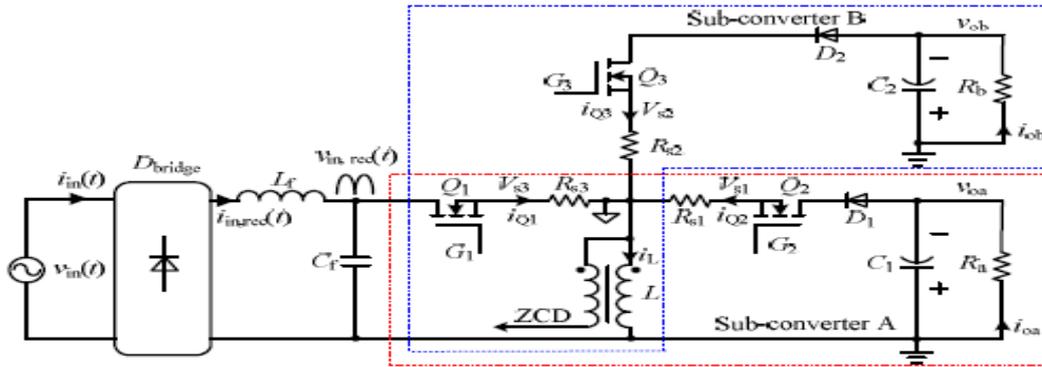


Fig.2. The proposed SIDO buck-boost PFC converter. Power stage

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III. DESIGN CONSIDERATIONS AND ANALYSIS

In this section, the SIDO buck-boost PFC converter operating CRM is analyzed under the following assumptions.

1) All the components as shown in Fig.2 are ideal. 2) The switching frequency f_{sw} is much higher than the line frequency $2f_L$, i.e. $f_{sw} \gg 2f_L$, input voltage can thus be considered as constant in a switching cycle. 3) The input voltage is a full-wave rectified sine wave, i.e., $v_{in,rec}(t) = |v_{in}(t)| = V_p |\sin(\omega t)|$, where V_p is the amplitude and $\omega = 2\pi f_L$ is the angular frequency of AC input voltage. 4) The output voltage v_{oa} and v_{ob} are constant, i.e., they have a negligible ac ripple in steady state. 5) As the bandwidth of the control loop of PFC converter is usually much lower than the rectified line frequency ($2f_L$), the error voltage of each output $v_e[i]$ ($i=1, 2$) are constant within each half of a line cycle, i.e., constant on time control can be achieved by controller.

IV. SIMULATION AND EXPERIMENTAL VERIFICATION

A 30.75W prototype of the proposed CRM SIDO buckboost PFC is built to verify the theoretical analysis. Each output current of the proposed CRM SIDO buck-boost PFC is constant. The prototype parameters. From (10), coefficient k is 0.49 to 0.20, with input voltage varying from 100Vac to 240Vac, which is higher than 0.19. Therefore, according to Fig.5, the harmonic current in prototype can meet IEC limit. According to the analysis, L is designed as 180uH. L_f and C_f , which are used to provide switching noise attenuation and achieve low displacement angle between input voltage and current [19], are seriously affected by F_{s_min} at low input voltage. Low F_{s_min} requires low cutoff frequency of input filter, which will increase the size of filter. In this paper, L_f and C_f are designed as 1mH and 220nF considering wide input voltage.

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TABLE
 CIRCUIT PARAMETERS OF SIDO BUCK-BOOST PFC CONVERTER

Variable	Definition	Value
V_{in}	Input voltage	100~240Vac
R_a	Rated load resistor of output A	300 Ω
I_{oa}	Current of output A	0.2A
R_b	Rated load resistor of output B	300 Ω
I_{ob}	Current of output B	0.25A
L	Inductor/Bobbin	180uH/RM8
Q_1	Power MOSFET	7N65
Q_2, Q_3	Multiplexing MOSFET	IRFR13N15D
D_1, D_2	Freewheeling diode	ES2J
L_f	Input filter inductor	1mH
C_f	Input filter capacitor	220nF
C_1, C_2	Output filter capacitor	220uF

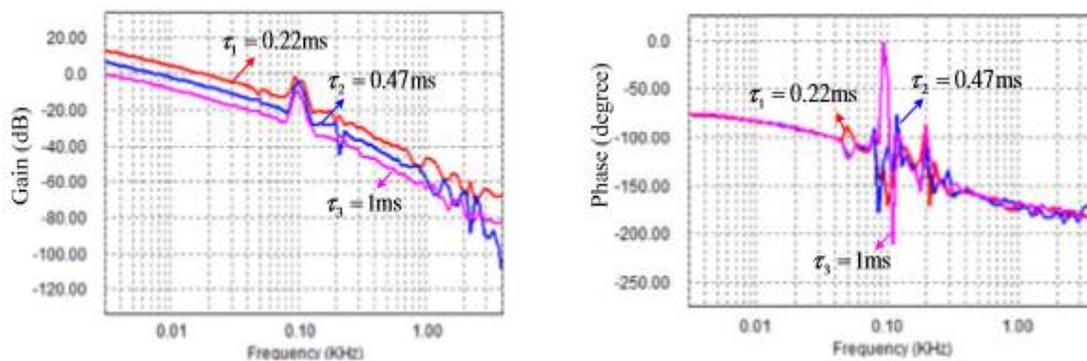


Fig.10. Loop gain simulation results of the sub-converter A with $\tau = Re3Ce3$.

According to Fig.2, low pass filter, Re_1 and Ce_1 , Re_2 and Ce_2 are used to filter inductor freewheeling current sense signal on Rs_1 and Rs_2 . Due to low frequency ($2fL$) ripple on Rs_1 and Rs_2 , the time constant of these low pass filters should be lower than $1/2fL$. The capacitance and resistance of these two filters are designed as 100nF and 120k Ω in this prototype. Two compensators (Op_1 , Re_3 , Ce_3 , Op_2 , Re_4 and Ce_4) are applied to achieve sufficient phase margin and low bandwidth for power factor correction. Fig.10 shows the loop gain of Psim simulation results at 100Vac for sub-converter A with different compensation parameters (τ_1 , τ_2 and τ_3) by using the circuit parameters shown in Table I. It can be observed that when time constant $\tau = Re3Ce3$ is lower than 0.22ms, the phase margin is approximately 90 degree when the compensator is applied. The bandwidth will be lower than 20Hz, which can ensure acceptable power factor correction requirement, but this low bandwidth severely affects the control loop dynamics [20], [21]. Poor transient performance will also cause poor transient cross-regulation performance. Therefore, the control loop design is a trade-off between PF and transient performance. The simulation result of transfer function with 50Hz ac input shows fluctuations at frequencies around 100Hz.

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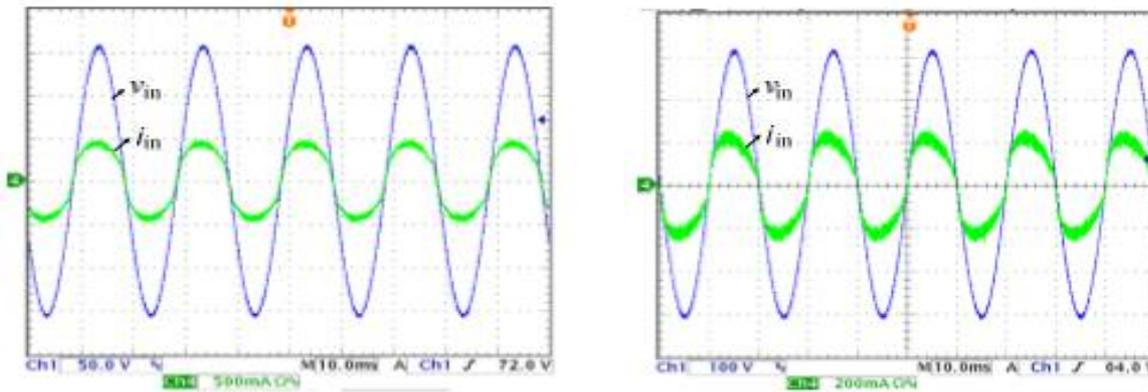
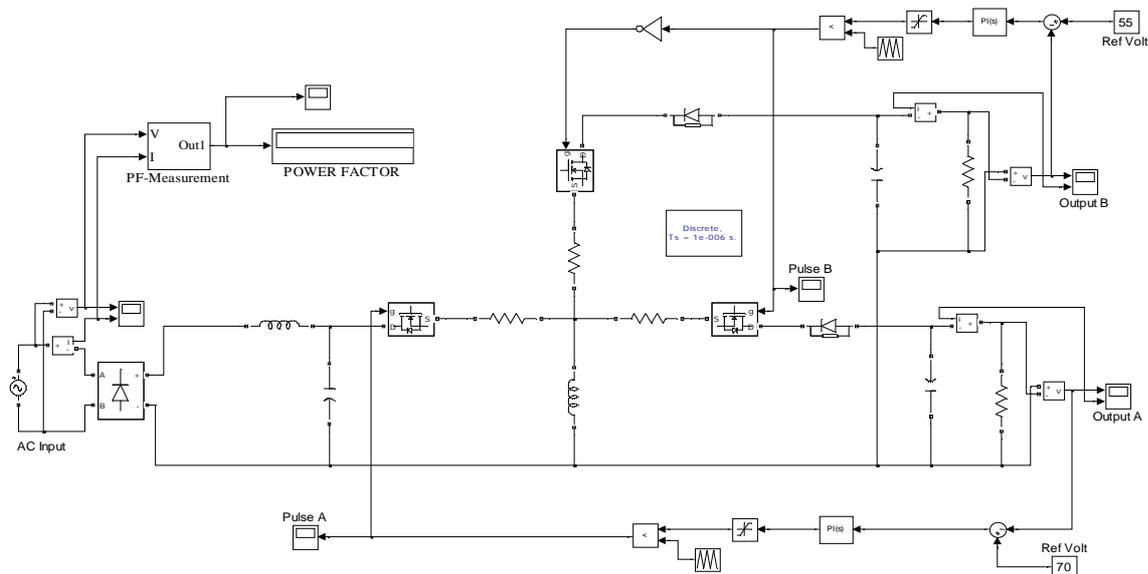


Fig.11 v_{in} and i_{in} waveforms of SIDO buck-boost PFC Converter at 110Vac input
Fig.12 v_{in} and i_{in} waveforms of SIDO buck-boost PFC Converter at 220Vac input

This fluctuation is due to the combined effects of 100Hz switching at the bridge rectifier and the 100Hz ripple in the output voltage. In order to make the design simple, the same compensation parameters are applied in two compensation network and the compensation parameters are designed as $Re3=Re4=10k_{\Omega}$, $Ce3=Ce4=47nF$ considering high PF and acceptable transient performance, i.e., $\tau_c=0.47ms$. The steady-state input current waveforms of CRM SIDO buck-boost PFC converter at rated output power are shown in Fig.11 and Fig.12. From Fig.11 and Fig.12, it can be known that input current i_{in} is in phase with input voltage v_{in} . The power factor correction function is achieved.

V. SIMULINK



In electrical engineering, the power factor of an AC electrical power system is defined as the ratio of the real power flowing to the load to the apparent power in the circuit,^{[1][2]} and is a dimensionless number in the closed interval of -1 to 1. A power factor of less than one means that the voltage and current waveforms are not in phase, reducing the instantaneous product of the two waveforms ($V \times I$). Real power is the capacity of the circuit for performing work in a particular time. Apparent power is the product of the current and voltage of the circuit. Due to energy stored in the load and returned to the source, or due to a non-linear load that distorts the wave shape of the current drawn from the source, the apparent power will be greater than the real power.

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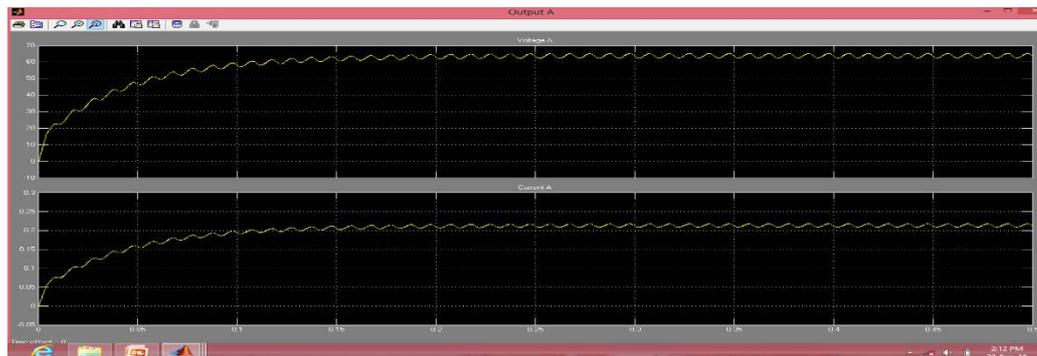
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Experimental results



a) Proposed the hardware structure

Wave Form A



b) Output voltage and current 1

c)

The above diagram discussed about the wave form difference between current and voltage. the voltage and current waveforms differs only by varying the value in reference voltage. The circuit configuration of multiple output ac/dc converter shown in Fig.1 is complex and suffers from high cost, with multiple inductors and controllers are required [6],[7]. Moreover, the two-stage power conversion with PFC pre regulator and dc-to-dc converters suffer from lower efficiency and higher volume and cost. However, single-stage PFC converter can achieve high PF and output current or voltage regulation at the same time [8], [9]. Hence, it has drawn more and more attention in recent years. Flyback PFC converter with multiple secondary windings is a typical single-stage multiple outputs converter, with only one output can be well regulated. Multiple secondary windings in the transformer leads to cross-regulation due to leakage inductance, forward voltage drop of diodes, and series resistance of the windings.

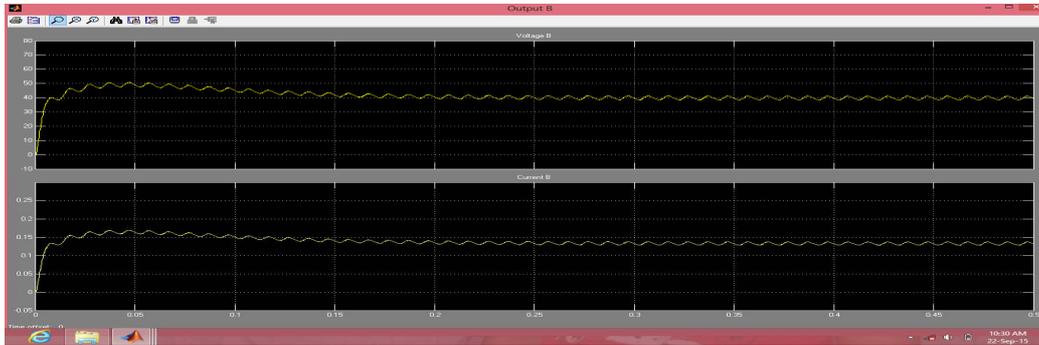


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Wave Form B



C) output voltage and current 2

The above diagram discussed about the wave form difference between current and voltage. the voltage and current waveforms differs only by varying the value in reference voltage.

V. CONCLUSION

A single-inductor dual-output buck-boost PFC converter operating CRM is proposed in this paper. Detailed control strategy analysis and design considerations are presented. Each output can be regulated independently in this converter by multiplexing a single inductor. Compared with conventional two-stage multiple output ac/dc converters, the proposed single-stage multiple output ac/dc converter benefits from significant overall cost saving, small size and light weight of device. Experimental results are presented to verify the analysis results, and demonstrate the advantage of the proposed converter. Although only dual-output converter is discussed in detailed in this paper, the proposed converter can be easily extended to realize SIMO PFC converters with different topology to fulfil different system requirements.

REFERENCES

- [1]. Jae-Kuk Kim, Seong-Wook Choi, Chong-Eun Kim, and Gun-WooMoon, "A new standby structure using multi-output full-bridge converter integrating flyback converter," *IEEE Trans.Ind. Electron.*, vol.58, no.10, pp. 4762-4767, Oct. 2011.
- [2]. Qu Xiaohui, Siu-Chung Wong, and Chi-K.Tse, "Noncascading structure for electronic ballast design for multiple LED lamps with independent brightness control," *IEEE Trans.Power Electron.*, vol.25, no.2, pp. 331- 340, Feb. 2010.
- [3]. Jesús Cardesín , Javier Ribas, Emilio López corominas, and Marco Antonio Dalla Costa, "LED permanent emergency lighting system Based on a single magnetic component," *IEEE Trans.Power Electron.*, vol.24, no.5, pp. 1409-1416, May. 2009.
- [4]. *Electromagnetic Compatibility (EMC), Part 3-2: Limits-limits for harmonic current emissions (equipment current _ 16 A per phase)*, International Standard IEC 61000-3-2, 2009.
- [5]. Manuel Arias, Diego G. Lamar, Francisco F. Linera, Didier Balocco, Almadidi Aguisa Diallo, and Javier Sebastián, "Design of a softswitching asymmetrical half-bridge converter as second stage of an LED driver for street lighting application," *IEEE Trans.Power Electron.*, vol.27, no.3, pp. 1608-1621, Mar. 2012.
- [6]. Huang-Jen Chiu, and Shih-Jen Cheng, "LED backlight driving system for large-scale LCD panels," *IEEE Trans.Ind. Electron.*, vol.54, no.5, pp. 2751-2760, Oct. 2007.
- [7]. Quanming Luo, Shubo Zhi, Can Zou, Weiguo Lu, and Luwei Zhou, "A LED driver with dynamic high frequency sinusoidal bus voltage regulation for multi-string applications," *IEEE Trans.Power Electron.*, vol.29, no.1, pp. 491-500, Jan. 2014.
- [8]. Chi K. Tse, Martin H. L. Chow, and Martin K. H. Cheung, "A family of PFC voltage regulator configurations with reduced redundant power processing," *IEEE Trans.Power Electron.*, vol.16, no.6, pp. 794-802, Nov. 2001.
- [9]. Beibei Wang, Xinbo Yuan, Kai Yao, and Ming Xu, "A method of reducing the peak-to-average ratio of LED current for electrolytic capacitor-less AC-DC drivers," *IEEE Trans.Power Electron.*, vol.25, no.3, pp. 592-601, Mar. 2010.