

International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 3, March 2015

Compact UWB-MIMO Antenna for Portable Devices

Linto Vasu¹, A.K Prakash²

PG Student [Wireless Technology], Dept. of ECE, Toc H Institute of Science and Technology, Kerala, India¹ Professor, Dept. of ECE, Toc H Institute of Science and Technology, Kerala, India²

ABSTRACT: A compact printed ultra-wideband (UWB) multiple input-multiple-output (MIMO) antenna system with a size of 35×60 mm² operating at a frequencyrange of 3.1–10.6 GHz is proposed. The wideband isolation can beachieved through a tree-like structure on the ground plane. Simulated S-parameters how that the isolation is better than -16 dB (-20 dB inmost of the band) across the UWB of 3.1–10.6 GHz. The radiation patterns, gain, and envelope correlation coefficient are also simulated. The proposed antenna is suitable for some portable MIMO/diversity applications.

KEYWORDS: Diversity, isolation, multiple-input-multiple-output (MIMO), ultra wideband (UWB) antennas.

I.INTRODUCTION

Multiple-Input Multiple-Output (MIMO) has proved itself as animportant technique for wireless communication systems. Using MIMO, wireless system's capacity or the range canbe increased signicantly [1]. On the other hand, Ultra Wideband (UWB) technology is a potential candidate in the race of the wirelessworld since the Federal Communications Commission (FCC) released are port for approving the use of UWB devices operating in the 3.1-10.6 GHz frequency range [2]. But this technology is limited to short-range communications due to extremely low allowable transmittedpower, i.e., 41.3 dBm/MHzto overcome this limitation, the combination of MIMO techniques with UWB technology is found to be ne of the solutions. However, another bottleneck while implementing the MIMO technique for compact or portable devices arises from the poor isolation and strong mutual coupling between the closely packedantenna elements. Both mutual coupling and isolation can be improved by increasing the distance between the antenna elements but the compact size of the wireless devices limits this approach. Therefore, a good challenge appears to enhance the isolation or to reduce themutual coupling by using some other technique. To combat the multipath fading problem in an indoor UWB wireless communication system, an UWB diversity antenna system is a promising candidate. Both MIMO and diversity UWB systems require an increase of the isolation among antennas. At the same time, the MIMO/diversity UWB antennas should be compact enough for portable devices. Therefore, compact MIMO/diversity UWB antenna systems with low mutual coupling among antenna elements are desirable for practical portable MIMO/diversity UWB applications. Many studies have been made to reduce the size of the antennas and increase the isolation and impedance bandwidths for MIMO/diversity UWB antenna systems [3]-[6].In [3], aUWB diversity monopole antenna has been designed, and aT-shaped reflector has been inserted between the two radiatorsto reduce the mutual coupling. Another diversity UWB antenna has been proposed in [4], and the impedance bandwidth is 3.1–5.8 GHz. Theisolation can be enhanced through a slot etched on a T-shapedreflector. In [5], a diversity antenna for PDA application hasbeen proposed, and it covers the band of 2.27-10.2 GHz. Threestubs have been introduced to weaken the mutual coupling. In [6], a coupling element is added between two closely packed antennas to improve the isolation. A neutralization technique to enhance port-to-port isolation is presented in [7] for two PIFAstructures.Lowmutual coupling is also difficult to achieve in the whole UWBwith the decoupling structure in [8]. In this letter, we propose a compact UWB MIMO/diversity antenna system. The designed antenna system has a small size of 35×60mm² and can cover the whole UWB (3.1–10.6 GHz). Through a tree-like structure, the measured isolation better than -16 dB in the whole UWB (-20 dB in most of the band) can be achieved.



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 3, March 2015

II.ANTENNA GEOMETRY AND DESIGN

The proposed UWB-MIMO antenna consisting of two radiating elements is illustrated in Fig.1a circular disc monopole fed by 50-micro stripline is used to develop the proposed UWB-MIMOantenna. The selection of this antenna can be justified by its goodperformance, size, and ease of integration. Antenna is optimized in this paper using FR4 substrate having relative permittivity of 4.4,0.8mm thickness and 0.02 dielectric losses. The individually optimized antenna elements are placed on a single substrate and are studied again parametrically and then optimized. The distance between the two radiators is only 35 mm. Each radiator is fed with a 50- microstripline. The wideband isolation between the two UWB radiatorscan be efficiently enhanced by a tree-like structure that extends from the ground plane.

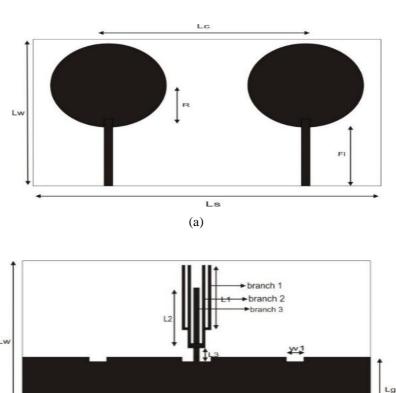


Fig.1 Geometry of the proposed UWB MIMO/diversity antenna system: (a) top view, (b) back view. Dimensions of antenna is given by the table as shown.

R	Lw	Ls	Fl	Lc	L1	L2	L3	W1	Lg
10	35	60	13.7	35	5	5	1.5	1	13.2

(b)

Table 1.Detailed dimensions (in mm) of antenna



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 3, March 2015

III.EFFECTIVENESSOF THE TREE-LIKE STRUCTURE

A wideband isolation can be achieved with the tree-like structure. Branch 1 [see Fig.2] can be viewed as a reflector, which can reduce the wideband mutual coupling through separating the radiation patterns of the two radiators. When the number of branches of tree like structure increases, mutual coupling further can be reduced and more resonance will be introduce. The wide band isolation can be efficiently enhanced as the resonances are in different frequency range.

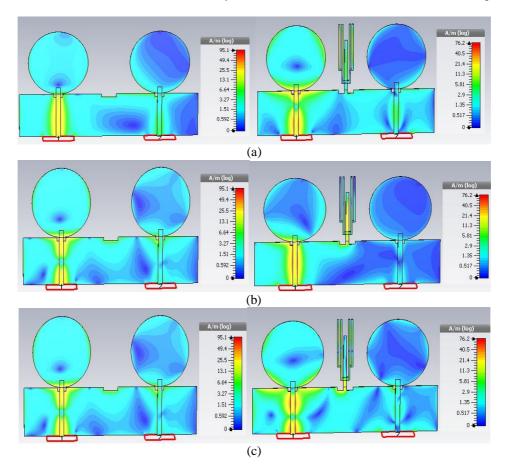


Fig. 2Surface current distributions with Port 1 excitation: (a) 4, (b) 7, and (c) 10 GHz.

In Fig.2, We can see that the surface current distribution at 4,7and 10 GHz are in fig.3 with and without the tree like structure. When port 1 is excited, the current from it is blocked by tree like structure and cannot flow to the other radiator through the ground plane. The effect is same when port 2 is excited. From the result we can see that the tree like structure can efficiently enhance the isolation between the radiators across the whole UWB.



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 3, March 2015

IV.RESULT AND DISCUSSION

A.Impedence performance

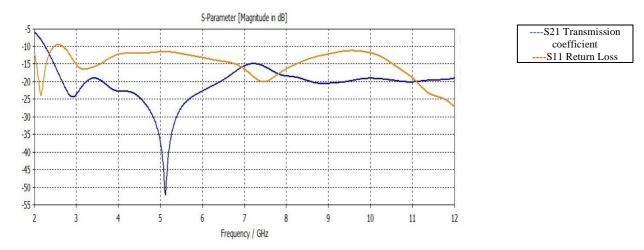


Fig.3simulated S-parameters of the UWB-MIMO antenna system.

Simulated S-parameters for the proposed UWB MIMO/diversity antenna system are shown in Fig.3. Impedance bandwidth (S11<-10dB) can cover the whole UWB of 3.1–10.6 GHz, and an isolation of more than -16 dB (more than -20 dB in most of the band) in the whole UWB is achieved.

B.Radiation pattern

The radiation patterns are measured at 4, 7, and 10 GHz and shown in Fig. 4.The radiation patterns of the designed antenna are relatively stable across the UWB. The antenna gives almost monopole radiation pattern throughout the bandwidth.

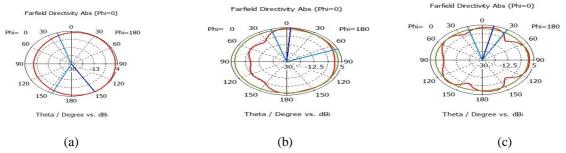


Fig.4Radiation patterns simulated at frequencies of(a)4 GHz, (b)7.0 GHz and (c)10 GHz.

C.Diversity performance

For a two-portsystem in uniform propagation environment, the envelope correlation coefficient ρ_{ν} can be simply calculated by



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 3, March 2015

$$\rho_{V=} \frac{|S11^*S12 + S21^*S22|^2}{(1 - (|S11|^2 + |S21|^2))(1 - (|S22|^2 + |S12|^2))} (1)$$

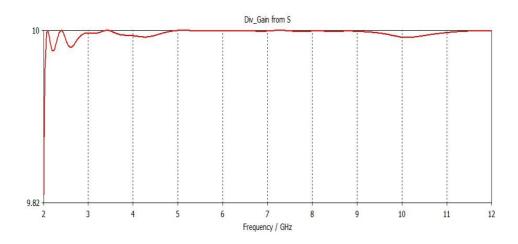


Fig.5 simulated Envelope correlation coefficient (b) Diversity Gain

In fig.5, The Envelope correlation coefficient for UWBMIMO/diversity antenna, obtained from the measured S-parameters and it is below 0.01 across the whole UWB of 3.1–10.6 GHz.

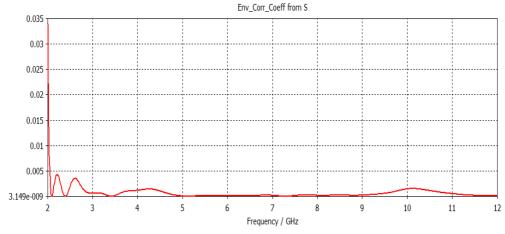


Fig.6 simulated Diversity Gain

The diversity gain (1%) has also been calculated and is larger than 9.95 dB across the whole UWB of 3.1–10.6 GHz as shown in fig.6. These indicate that the designed antenna has a good MIMO/diversity performance.

D.Time domain performance

The radiating elements of the designed UWB-MIMO antenna are also characterized for its time domain performance to confirm their capability for UWB operations. The radiating elements are fed bythe fifth derivative of Gaussian pulse of 0.13 ns wide where the pulsewidth is measured at 50% of the maximum amplitude. The selection of this excitation pulse can be justified by its spectrum that efficiently meets the requirements of FCC approved UWB spectral mask.



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 4, Issue 3, March 2015

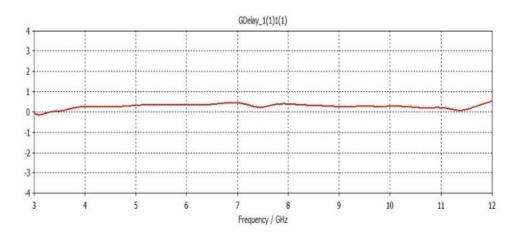


Fig.7simulated group delay

It indicates good time domain response and it can be further justified by group delay shown in Fig.7. The variation of group delay is found to be less than 1 ns showing good phase linearity and thus it fulfils the requirement for UWB operations.

V.CONCLUSION

Compact MIMO antenna for Ultra-Wideband applications is designed and simulated. The wideband isolation can be achieved through anappropriately designed tree-like structure. The effectiveness of the tree-like structure has been shown. The obtained impedancebandwidth of designed antenna can cover the wholeUWBof3.1–10.6 GHz.Within the UWB, the measured isolation is better than 15 dB in the whole band and 20 dB in most of the band. The radiation patterns, antenna gain, envelope correlation coefficient, and time domain response have also been simulated. The simulated resultshave shown that the proposed antenna system is very suitable for portable MIMO/diversity applications.

REFERENCES

- [1] 1. Foschini, G. J. and M. J. Gans, "On limits of wireless communications in a fading environment when using multiple antennas," Wireless Personal Communications, Vol. 6, No. 3, 311{335, 1998.
- [2] Federal Communication Commission (FCC), \Revision of part 15 of the commission's rules regarding ultra-wideband transmission systems," ET Docket 98{153, FCC 02{48, First Report and Order, Apr. 2002.R.
- [3] K. L. Wong, S. W. Su, and Y. L. Kuo, "A printed ultra-wideband diversity monopole antenna," *Microw. Opt. Technol. Lett.*, vol. 38, no. 4, pp. 257–259, 2003.
- [4] L. Liu, H. P. Zhao, T. S. P. See, and Z. N. Chen, "A printed ultra widebanddiversity antenna," in Proc. Int. Conf. Ultra-Wideband, Sep. 2006, pp. 351–356.
- [5] S. Hong, K. Chung, J. Lee, S. Jung, S. S. Lee, and J. Choi, "Designof a diversity antenna with stubs for UWB applications," *Microw. Opt. Technol. Lett.*, vol. 50, no. 5, pp. 1352–1356, 2008.
- [6] T. S. P. See and Z. N. Chen, "An ultra-wideband diversity antenna," *IEEE Trans. Antennas Propag.*, vol. 57, no. 6, pp. 1597–1605, Jun. 2009.
- [7] Dossche, S., S. Blanch, and J. Romeu, "Optimum antenna matching to minimize signal correlation on a two port antennadiversity system," Electronic Letters, Vol. 40, No. 19, 1164{1165,Sep. 2004.
- [8] T. S. P. See and Z. N. Chen, "An ultra-wideband diversity antenna," IEEE Trans. Antennas Propag., vol. 57, no. 6, pp. 1597–1605, Jun. 2009.