



# **Investigation of Severity of Lung Fibrosis By Dynamic Modelling Of Human Respiratory System**

**Shamik Saha<sup>1</sup>, Subhabrata Mukherjee<sup>2</sup>**

B.Tech Student, Dept. of AEIE, Heritage Institute of Technology, Kolkata, West Bengal, India <sup>1</sup>

B.Tech Student, Dept. of AEIE, Heritage Institute of Technology, Kolkata, West Bengal, India <sup>2</sup>

**ABSTRACT:** In this work, the severity of lung fibrosis is assessed by developing an electric model. This model is an electrical analogy to the biological structure of the human respiratory system. The electrical model composes of resistors (R), capacitors (C) and inductors (L). Different computational studies can be carried out by developing a transfer function from this model. This facilitates qualitative investigations and assessment of the various stages of severity of lung fibrosis. Various tools (like state space modelling) have been adopted by us in order to verify the validity of the proposed model. The physiological status of alveoli conditions of the lungs are observed by computing both the time and frequency domain responses. The alveolar compliance of the lungs determines the criticality of pulmonary scarring or fibrosis.

**Keywords-** fibrosis; respiratory system; electrical mode; time/frequency-domain responses; state-space technique; stability analysis; compliance.

## I. INTRODUCTION

The potential causes of lung fibrosis maybe due to inhalation of asbestos, ground stone or metal dust; however if the cause is unknown then the condition is called idiopathic lung fibrosis. For the past two decades it has been observed that probability of death from pulmonary fibrosis is increasing rapidly with age [1-3]. According to, American Thoracic Society and the European Respiratory Society, the most common cause of death is progressive lung disease (60% of deaths) and among which idiopathic lung fibrosis is very common [4-5].

Researchers have proposed various models to study the breathing performance relating lung compliance and air tract resistance. Graham Sturton et al. showed that changes in the physiological structure of the minute airways (<2 mm diameter) were mostly responsible for Chronic Obstructive Pulmonary Diseases (COPD) [6]. In 2006, B. Diong et al. described an electric circuit based model of the respiratory system that helps the detection and diagnosis of various obstruction related diseases of human respiratory system [7]. P. Segers and R. De Keyser proposed a technique to provide the mechanical parameters of the respiratory airways (resistance, inertance, and compliance) from morphological insight to enable the correlations of fractional-order models with pathologic changes. The investigators formulated a set of equations taking into account the various anatomical aspects, such as, inner radius, wall thickness, tube length, and tissue structure of each airway level to effectively model the pressure drop, wall elasticity, flow, and air velocity (both axial and radial). They studied the effects of pulmonary diseases which affect the inner radius and elastic modulus of bronchial tree [8].

A theoretical model of sound transmission from within the respiratory tract to the chest wall due to the motion of the walls of the large airways was proposed by K. N. Stevens et al.. The vocal tract, trachea, and first five bronchial generations were implemented over the frequency range from 100 to 600 Hz by an equivalent acoustic circuit. This circuit made it possible to

estimate the magnitude of airway-wall motion in response to an acoustic perturbation at the mouth. The model estimates the magnitude of acceleration over the extra thoracic trachea and at three locations on the posterior chest in the same vertical plane.



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The predicted spectral characteristics of transmission corroborate with the previous experimental observations [9]. Clara Ionescu, Eric Derom, Robin De Keyser, in January 2010, for assessment of respiratory mechanical properties [6, 12]. A complex formula of an iterative, weighted nonlinear least squares method of parameter estimation of the human respiratory system was proposed to provide physiological data to the performance of the breathing system [10]. T. Sbrana et al. In the year 2011, proposed a model to simulate exhalation phase in human respiratory system which mimics the bronchial resistances of human's lung in during expiration in MATLAB environment. The inputs to this model were the spirometric values [11]. The fractional-order modelling was introduced in clinical studies of ventilator diseases where the structural changes in lung components were correlated for diagnosis of lung where the inertia of airflow, compliance of trachea and resistance offered by the respiratory tract were compared with an inductor, a capacitor, and a resistor respectively.

In this paper, the human ventilatory system has been represented through an electrical model which has been simulated for assessment of the severity of fibrosis in the lungs. So as to assess the ventilatory performance, lung compliance (C) and airway resistance (R) are two vital lung parameters. Here, we have also considered inertia of the air flow, whose electrical analogy is inductance (L). For this purpose, the lung ventilator model is developed in the form transfer function comprising of R, L and C. This driving pressure which allows the air flow in and out of the lungs is considered the differential pressure between the atmospheric pressure and alveolar pressure. For analysing fibrosis in lungs, we have simulated the electrical model for three different lung conditions as i) normal ii) affected and iii) highly affected by varying the compliance of lungs.

The paper is divided four sections beginning with electrical modelling of respiratory system. The following section introduces the respiratory problems associated with fibrosis. The third one deals with validation of our proposed model of the breathing system by application of state space analysis technique. In results and discussions section, we have enriched our study by using Bode plots where a correlation between phase margin and alveolar compliance has been shown. The conclusion of this work is discussed briefly in the fourth section.

## II. ELECTRICAL MODELING OF RESPIRATORY SYSTEM

Fig. 1 showcases the physiological structure of lungs and airways whose equivalent electrical circuit is represented in Fig. 2. In Fig. 2, the trachea (an airway with largest cross section area among the respiratory airways) is represented by electrical resistance  $R_t$ , air-flow inertia is indicated by  $L_t$ ,  $R_{b1}$  and  $R_{b2}$  are meant for the main bronchi (both left and right with smaller cross sectional areas relative to trachea), whereas, air-flow inertia in the bronchi are characterized by  $L_{b1}$  and  $L_{b2}$  (electrical inductances). The assembly, comprising of bronchioles and cluster of alveoli (Fig. 1) is a series connection of a resistor  $R_v$  and an effective capacitor  $C_v$  in Fig.2.

## III. RESPIRATORY PROBLEMS ASSOCIATED WITH LUNG FIBROSIS

Lung fibrosis, also referred to as pulmonary fibrosis, is a clinical condition that occurs when the alveoli, or air sacs, become inflamed and scarring develops on the lung tissue. Due to scarring of the air sacs, the lung tissue is gradually replaced by air fibrous tissue. Fibrous tissue is thicker and stiffer, so it prevents the sacs from inhaling oxygen.

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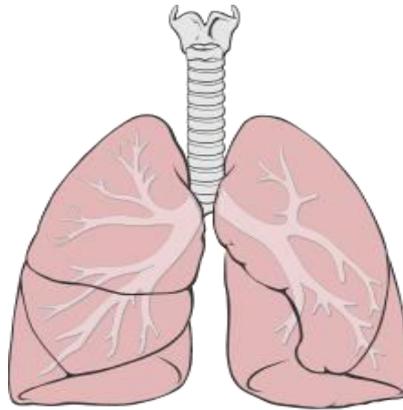


Fig 1: Structure of lungs and airways [18].

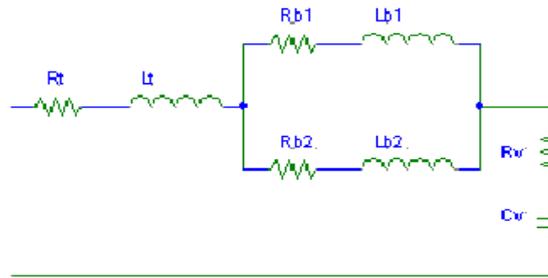


Fig2:Equivalent Electrical model of the respiratory system

The alveolar elasticity is described through its compliance whose electrical analog is capacitance (Fig. 2).

#### IV. MATHEMATICAL REPRESENTATION OF THE TRANSFER FUNCTION

$$\frac{V_o(s)}{V_i(s)} = \frac{R_v + \frac{1}{C_v s}}{R_t + L_t s + R_{be} + L_{be} + R_v + \frac{1}{C_v s}}$$

$$= \frac{R_v C_v s + 1}{s [(L_t + L_{be})s + (R_t + R_{be} + R_v)C_v]}$$

where,  $R_e$  and  $L_e$  stand for the effective resistance and inductance of the bronchi (left and right) respectively,  $V_o$  and  $V_i$  indicate the alveolar and atmospheric pressures respectively.

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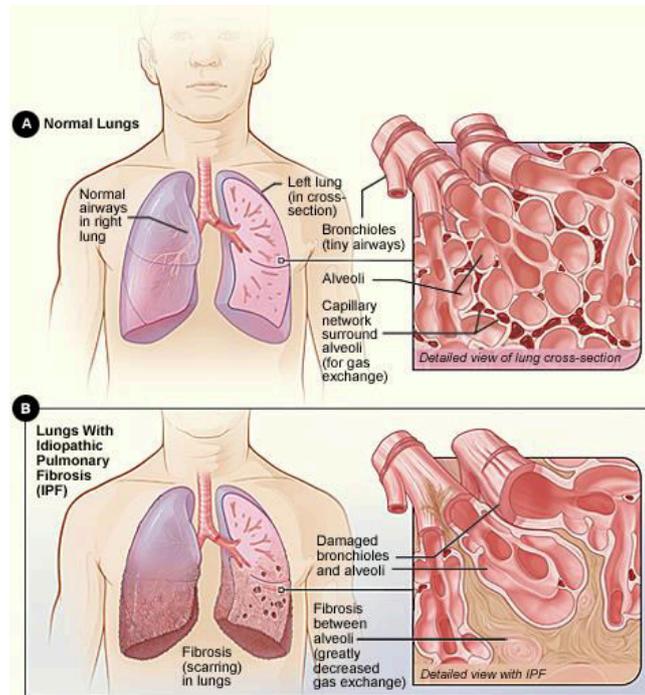


Fig.3: Status of alveoli due to fibrosis in lungs [19]

## V. VALIDATION OF PROPOSED ELECTRICAL MODEL

### A. To study lung fibrosis through state space technique

We have observed the responses of the respiratory system for pulmonary fibrosis with three different stages. i) healthy i.e. normal ii) affected and iii) severely affected alveoli. For normal lung conditions, we have chosen that the air ways impedances are constant and the electrical compliance is averaged with  $C_v=0.01$  Liter/cm of  $H_2O$ .

*Stage1: Stating the patient's alveoli are in healthy condition (normal)*

We have studied the performance of the respiratory system using state space model by taking values of  $R_t=4.5$  cm of  $H_2O$ -sec./ liter,  $R_e=9$  cm. of  $H_2O$ -sec./liter,  $R_v=15$  cm. of  $H_2O$ -sec./liter,  $L_t = 0.043$  cm of  $H_2O$ -sec.<sup>2</sup>/liter,  $L_e =0.17$  cm. of  $H_2O$ -sec.<sup>2</sup>/liter,  $C_v=0.01$  Liter transfer function is

$$\frac{V_o(s)}{V_i(s)} = \frac{0.15s + 1}{s(0.213s + 0.285)} \quad (2)$$

By using the concept of state space model, we have computed the following matrices (derived from Eq. 2). The respiratory system matrix is evaluated as

$$A = \begin{bmatrix} -1.338 & 0 \\ 1.000 & 0 \end{bmatrix}$$



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The input and output matrices of the respiratory system

$$B = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \text{ and } C = [0.7042 \quad 4.6942] \text{ respectively.}$$

Finally the Eigen values of the system are figured as 0 and -1.3380.

### Stage2: Stating alveoli are in affected condition

In a similar technique, we have simulated the response of the affected alveolar condition using state space model. Here too, keeping the air tract impedances unchanged, we have changed the alveolar compliance to 0.001 Liter/cm of H<sub>2</sub>O. The transfer function is as

$$\frac{V_o(s)}{V_i(s)} = \frac{0.015s + 1}{s(0.213s + 0.0285)} \quad (3)$$

The simulation results are observed in terms of state space matrices. Thus, the respiratory system matrix

$$A = \begin{bmatrix} -0.1338 & 0 \\ 1.000 & 0 \end{bmatrix}$$

The input and output matrices of the respiratory system are found as

$$B = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \text{ and } C = [0.07042 \quad 4.6942] \text{ respectively.}$$

The Eigen values of the system we calculated as 0 and -0.1338.

### Stage3: Stating badly affected alveolar condition

The alveolar compliance reduces due to long-term exposure to a number of toxins and pollutants. By following the similar computational approach and choosing the value of Cv = 0.0001 Liter/cm of H<sub>2</sub>O in the transfer function (Eq.1), we get

$$\frac{V_o(s)}{V_i(s)} = \frac{0.0015s + 1}{s(0.213s + 0.00285)} \quad (4)$$

Simulation studies yield the respiratory system matrix as

$$A = \begin{bmatrix} -0.01338 & 0 \\ 1.000 & 0 \end{bmatrix}$$

And the input and output matrices are

$$B = \begin{bmatrix} 1 \\ 0 \end{bmatrix} \text{ and } C = [0.007042 \quad 4.6942] \text{ respectively.}$$

The Eigen values of the system we calculated as 0 and -0.01338.

The above results are summarized in Table-I.



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TABLE-I: SUMMARY OF THE OBSERVATIONS

Alveolar conditions	Value of the compliance in Liter/cm of H <sub>2</sub> O	Eigen values
Normal	0.01	0, -1.3380
Poor	0.001	0, -0.1338
Poorer	0.0001	0, -0.0134

The results show that Eigen values are indicative of the severity of the scarring of the lung tissue. As the Eigen values, which are the roots of the characteristic equation of the respiratory system, are approaching the origin of the complex s-plane, severity of the disease increases.

## VI. RESULTS AND DISCUSSIONS

We have further enriched our simulation process with Bode plots. Once again, we have classified the alveolar conditions as normal, affected and highly affected. Considering the airway-impedance same and alveolar compliance as  $C_v = 0.01$  Liter/cm of H<sub>2</sub>O, the Bode plots are observed as shown in the Fig. 4. The phase margin, which is a frequency domain specification, is used to assess the relative stability of the ventilator was figured as  $50.4^\circ$ . In second stage, we have chosen  $C_v$  as 0.001 Liter/cm. of H<sub>2</sub>O, for a distressed alveolar state, the Bode magnitude and phase plots were obtained as shown in the Fig. 5 showing a phase margin of the breathing system as  $PM=5.4^\circ$ . With  $C_v = 0.0001$  Liter/cm of H<sub>2</sub>O, in third stage, we have monitored the Bode plots as depicted in Fig. 6 for severely fibrosis affected patient. Phase margin was quantized as  $0.54^\circ$ .

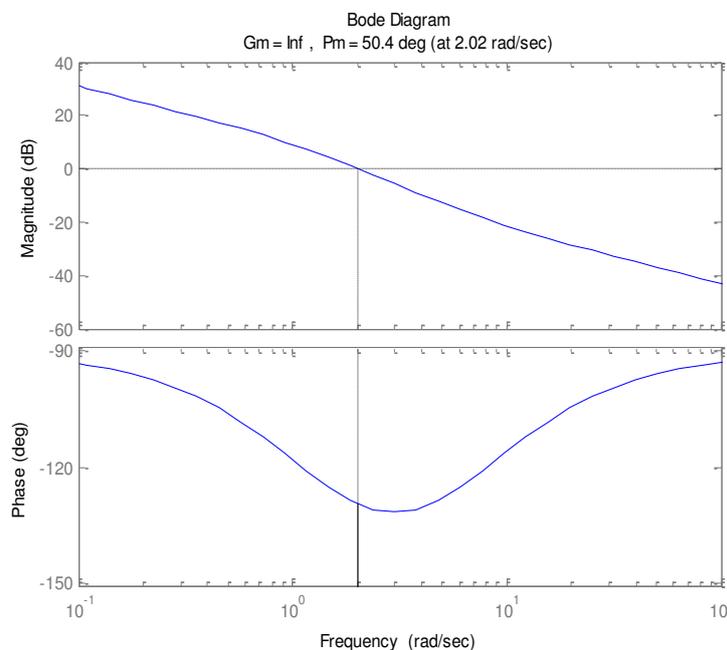


Fig. 4: Bode Plots for healthy alveolar condition

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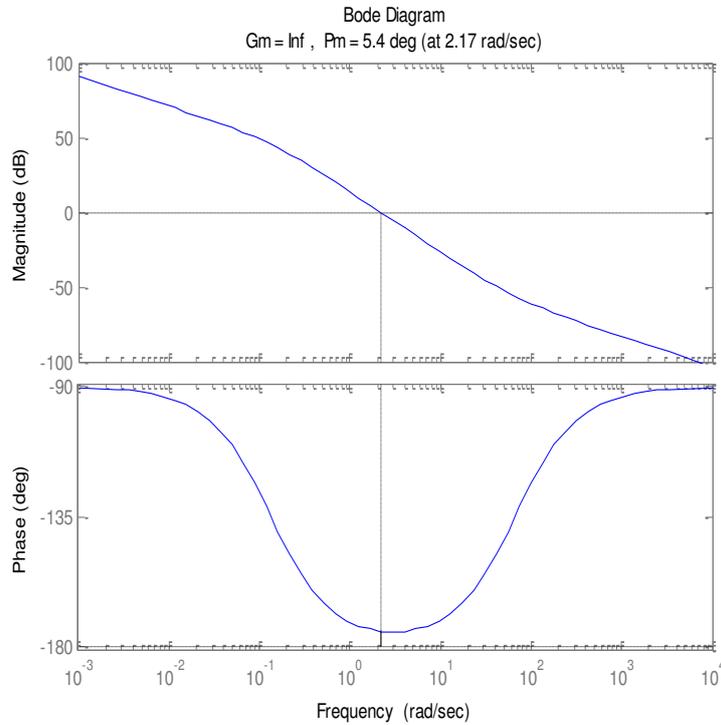


Fig. 5: Bode Plots for affected alveolar condition

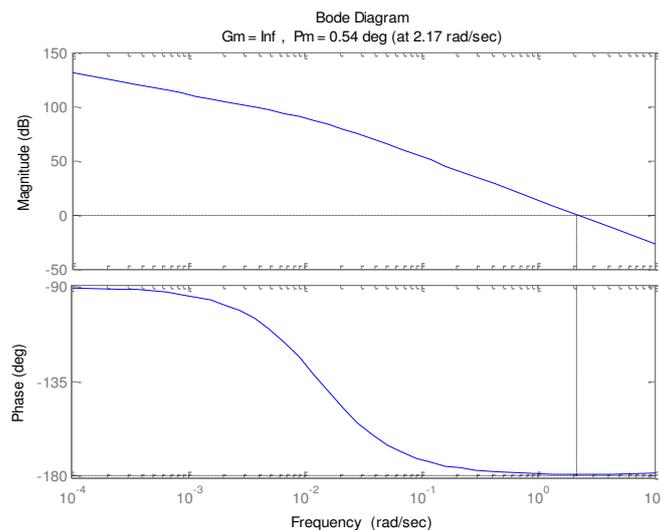


Fig. 6: Bode Plots for severely affected alveolar condition

As the phase margin is decreasing the severity of the fibrosis or scarring in the lungs is more. The simulation results are summarized in Table-II.



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TABLE II: SUMMARY OF THE OUTCOMES OF THE ANALYSIS THROUGH THE BODE PLOTS

Alveolar conditions	Value of the compliance Liter/cm of H <sub>2</sub> O	Phase Margin in Degrees
Normal	0.01	50.4
Affected	0.001	5.4
Severely affected	0.0001	0.54

## VII. CONCLUSION

In this work an electrical model consisting of passive components has been tested on three groups: healthy, affected and severely affected fibrosis patients. The main purpose of this work is to identify the differences in responses of a healthy individual and one with scarred lungs. The differences have been monitored and accumulated in tabular form. The influence of fibrous tissue on lungs have been assessed in terms of stability analysis

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