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# Extended Hybrid DC-DC Converter Adopting Voltage Multiplier Cell for High Voltage gain

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**ABSTRACT:** —Photovoltaic cells and fuel-cell stacks are examples of renewable energy sources that are growing rapidly around the world. The high voltage ratio boosting converter is becoming more popular due to the widespread use of renewable energy with low output voltage. This paper describes a voltage multiplier cell with a high step-up extensible hybrid DC-DC converter. A twophase interleaved boost converter, a switched capacitor (SC) boost circuit, and a voltage multiplier cell make up the converter. Two capacitors, two diodes, and one inductor make up the voltage multiplier cell. It is used on the converter's output side to boost voltage gain. High voltage gain, low switching voltage stress, and reduced input current ripple are all advantages of the converter. The converter's input current ripple was further decreased by increasing the number of parallel channels or SC units. The converter's performance is investigated using MATLAB/SIMULINK R2017a. The converter has 73% efficiency and a voltage gain of roughly 13.25, according to the simulation results

**KEYWORDS:** High step-up, interleaved, low input ripple, Voltage multiplier cell

## I.INTRODUCTION

The energy problem and environmental degradation have become more apparent in recent years. Photovoltaic cells and fuel-cell stacks are examples of renewable energy sources that are gaining traction around the world. The rapid expansion of renewable energy systems necessitates the creation of a new generation of high gain DC-DC converters that are both efficient and inexpensive. The front end of a "Plug and Play" PV system normally requires a step-up converter that can boost the voltage from 35V to 380V while maintaining regulation. [1] Presents an interleaved switch-capacitor based high step-up extensible hybrid DC-DC converter. A two-phase interleaved boost converter and a switch-capacitor (SC) boost circuit are used in the converter. Low switching voltage stress and reduced input current ripple are advantages of this converter. Because of their simple structure and great dependability, isolated high step-up DC-DC converters are frequently utilized; further, the voltage gain may be altered flexibly by modifying the transformer's turns ratio. However, a high turns ratio will invariably result in decreased efficiency and power density. When isolation is not required, the traditional boost converter is popular in many step-up applications. The converter has fewer parts and is simple to use. However, once the high boost ratio is achieved, the switch duty cycle will increase, causing a significant reverse recovery current spike in the output diode.

A very high switch duty cycle might also result in decreased efficiency and dependability. In terms of voltage stress and power density, high step-up converters with SC circuits perform better. In most cases, the inductor or input source charges the capacitors in the unit in one stage and discharges them in the next. Although the switched capacitor DC-DC converter has a high efficiency, it has pulsing current and weak regulation. The use of a resonant switched-capacitor converter can reduce pulsing current but does not address the issue of regulation. [4] Proposes a single-stage boost converter topology based on SC circuits. The converter works on the idea of parallel-charging-series discharging, which can aid with voltage rise. It maintains the benefits of a boost converter, reducing semiconductor voltage stress and input current ripple significantly. Nonetheless, in some situations, the voltage gain, which is just two times that of a normal boost converter, is insufficient. [3] Proposes a three-phase high step-up converter. This converter's voltage gain is larger than that of [4], However, the three inductors result in a bigger converter volume, and the three MOSFETs complicate design.

A hybrid boost converter circuit expansion technique proposed in [6]. The expansion concept will allow the converter to be used in a wider range of applications. Moreover, the converter's input current ripple is rather significant, which could damage the life of emerging energy sources like solar cells and fuel cells. An interleaved boost converter with



voltage multiplier cell is provided in this research. Low switching voltage stress and reduced input current ripple are advantages of this converter. This paper describes how to apply the voltage multiplier technique to a non-isolated DC-DC converter to achieve high voltage gain while reducing the converter’s voltage stress by lowering the maximum switch voltage. These features enable for high static gain and efficiency, allowing for the design of a compact circuit for applications that do not require isolation.

## II. WORKING PRINCIPLE

Fig. 1 depicts the proposed topology. A two-phase interleaved boost converter, switch-capacitor (SC) boost circuit and voltage multiplier cell are used in the proposed converter. One of the boost channels charges the capacitors in the SC circuit, while another boost channel supplies power to the load in series with the capacitors. The voltage multiplier cell is used on the converter’s output side. The converter provides excellent voltage gain, decreased semiconductor voltage stress, and lower input current ripple because of its arrangement.

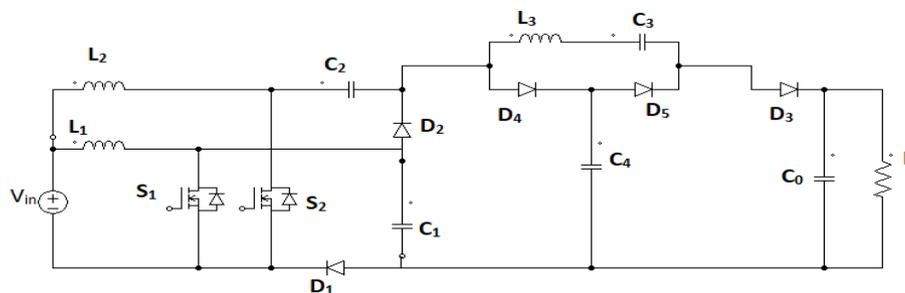


Fig. 1 The proposed circuit diagram

The inductor  $L_1$ , the switch  $S_1$ , the diodes  $D_1$ ,  $D_2$  and the capacitors  $C_1$ ,  $C_2$  constitute a boost converter and the inductor  $L_2$ , the switch  $S_2$ , the diode  $D_3$ , and the output capacitor  $C_0$  constitute another boost converter. The voltage multiplier cell consists of two diodes  $D_4$ ,  $D_5$ , inductor  $L_3$  and capacitors  $C_3$ ,  $C_4$ .

### 2.1 Modes of Operation

The switching period  $T_s$  is divided into four operating modes. The equivalent circuit of different working modes are explained below.

Mode 1: In this mode at time  $t = t_0$ , the switches  $S_1$  and  $S_2$  are both turned on. The inductors  $L_1$  and  $L_2$  are linearly charged by the input source  $V_{in}$ . Capacitor  $C_0$  supplies power to the load. Fig.2 shows the equivalent circuit diagram of the converter and current paths for this mode.

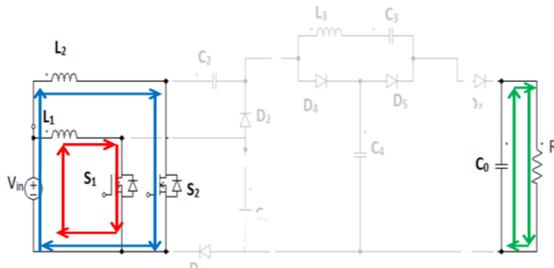


Fig. 2 Mode 1

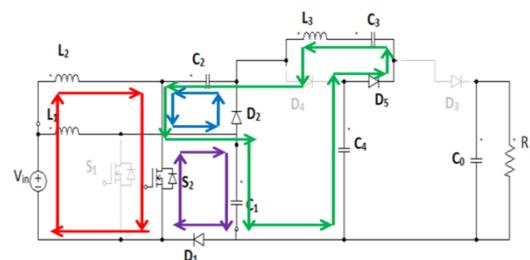


Fig. 3 Mode 2

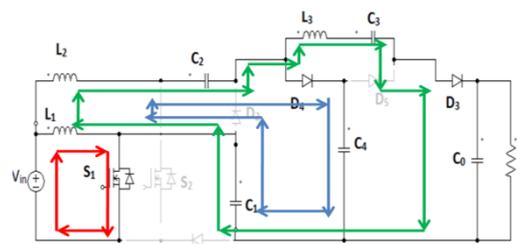


Fig. 4 Mode 4



Mode 2: At  $t=t_1$ , the switch  $S_1$  is turned off and  $S_2$  is turned on. The inductor  $L_1$  releases energy to the capacitors  $C_1$  and  $C_2$ , and current through  $L_1$  decreases linearly. At this time, there are two current paths. One is through the  $D_1, S_2$  to charge capacitor  $C_2$  and in other the inductor current charges capacitor  $C_1$  through  $D_1$ . Inductor  $L_2$  is charged by the input source  $V_{in}$  and the inductor current continues to rise linearly. Capacitor  $C_0$  supplies power to the load. In this mode capacitor  $C_3$  and  $C_2$  are discharged to charge  $L_3$  and  $C_3$ . Fig.3 shows the equivalent circuit diagram of the converter and current paths for this mode.

Mode 3: As shown in Fig. 2, this mode is same as mode 1.

Mode 4: In this mode at time  $t_0$ , the switch  $S_2$  is turned off and  $S_1$  continuous to conduct. At the same time inductor  $L_1$  is connected in series with  $V_{in}, C_1$  and  $C_2$  to supply power to the load through  $C_1$  and  $D_3, L_3$  and  $C_3$ . The voltage across  $L_1$  is same as that of the input voltage  $V_{in}$  and current of  $L_1$  continuous to rise linearly.

**2.2 Design Consideration of Main Components**

The input voltage is taken as 48 V. The pulses are switched at the rate of 100 kHz with a duty ratio of 0.631.

**A. Duty Cycle**

$$\frac{V_{out}}{V_{in}} = \frac{3}{1-D} \tag{1}$$

**B. Inductors**

$$L_1 = L_2 = \frac{D \cdot V_{in} \cdot T_s}{\Delta I_L} \tag{2}$$

$$L_3 = \frac{V_{out} - V_{C4}}{\Delta I_{L3}} \tag{3}$$

**C. Capacitors**

$$C_1 = \frac{(1-D) \cdot I_{L1}}{2 \cdot f_s \cdot \Delta V_{C1}} \tag{4}$$

$$C_2 = \frac{(1-D) \cdot I_{L2}}{2 \cdot f_s \cdot \Delta V_{C2}} \tag{5}$$

$$C_3 = C_4 \geq \frac{P_{max}}{V_{C3}^2 \cdot f_s} \tag{6}$$

$$C_0 = \frac{(1 - D) \cdot I_0}{f_s \cdot \Delta V_{C0}} \tag{7}$$

$\Delta V_{C1}, \Delta V_{C2}$  and  $\Delta V_{C0}$  are the maximum tolerant voltage ripple on the capacitors  $C_1, C_2$  and  $C_3$  respectively.  $\Delta I_{L2}$  is current ripple on input current. In order to design for operation in CCM and the inductor current ripple is assumed as 10% of input current. The inductor  $L_1, L_2$  is  $600\mu H$  and  $L_3$  is  $1\mu H$ . The capacitors  $C_1, C_2$  are designed as  $2.2\mu F$  and capacitor  $C_3, C_4$  and  $C_0$  are  $47\mu F$ .

$$\text{Input current } I_{in} = \frac{3I_0}{1-D} \tag{8}$$

**III. CONTROL STRATEGY**

The duty cycle of switches  $S_1$  and  $S_2$  are greater than 0.5 and interleaved with 180 degree phase shift is shown in Fig.5

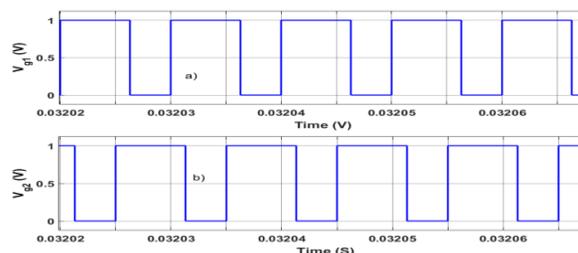


Fig. 5 Switching pulses to  $S_1$  and  $S_2$



IV. SIMULATION RESULTS

The proposed converter is simulated in MATLAB/SIMULINK by choosing the parameters listed in Table1 and the Simulink model is shown in Fig.6. The simulation results of the hybrid DC-DC converter are shown in the following figures.

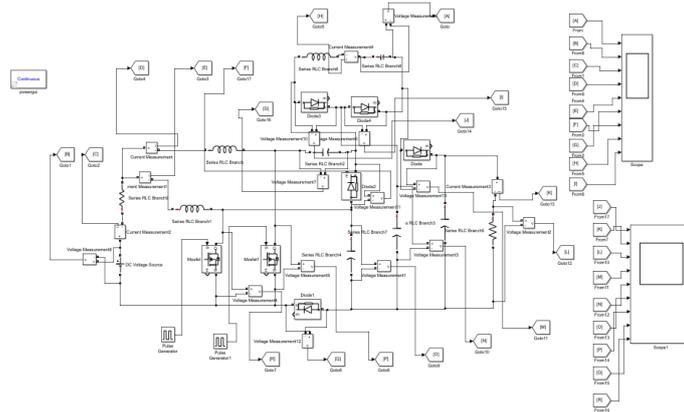


Fig. 6 Simulink model of converter

From Fig.7, it can be seen that the input voltage  $V_{in}$  is 48 V and the input current  $I_{in}$  is 7.14 A. The switching frequency is chosen to be 100 kHz and the duty ratios of  $S_1$  and  $S_2$  is equal to 0.631. The output voltage  $V_{out}=637$  V and  $\Delta V_{out}=0.08$ ,  $I_{out}=0.4412$  A and  $\Delta I_{out}=0.00005$  A.

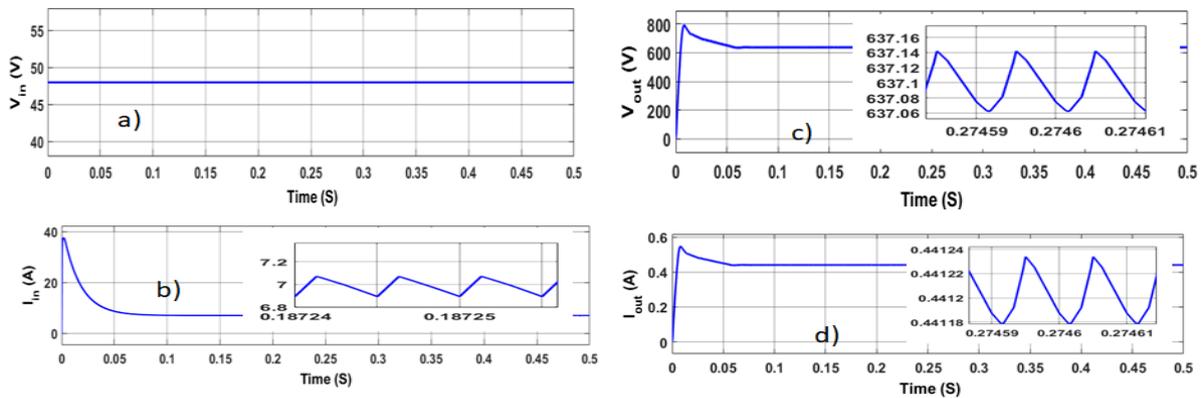


Fig. 7 a) Input voltage b) Input current c) Output voltage d) Output current

Fig.8 shows the current through inductor. Current through inductor with  $I_{L1}= 5$  A and  $\Delta I_{L1}=0.4$  A,  $I_{L2}= 3.8$  A and  $\Delta I_{L2}=0.4$  A,  $I_{L3}=2.2$ A.

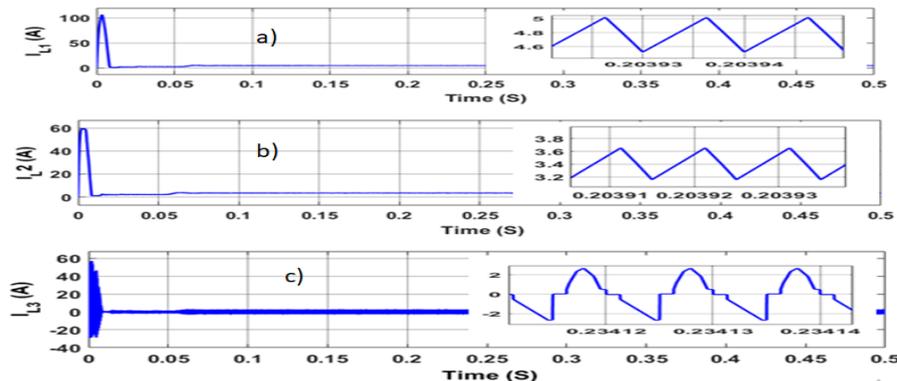


Fig. 8 Inductor current a)  $I_{L1}$  b)  $I_{L2}$  c)  $I_{L3}$



Fig.9 shows the voltage across capacitors with magnitude  $V_{C1}=129.7\text{ V}$  and  $\Delta V_{C1}=1.3\text{ V}$ ,  $V_{C2}=129.7\text{ V}$  and  $\Delta V_{C2}=0.8\text{ V}$ ,  $V_{C3}=255\text{ V}$  and  $\Delta V_{C3}=0.1\text{ V}$ ,  $V_{C4}=382\text{ V}$  and  $\Delta V_{C4}=0.1\text{ V}$ .

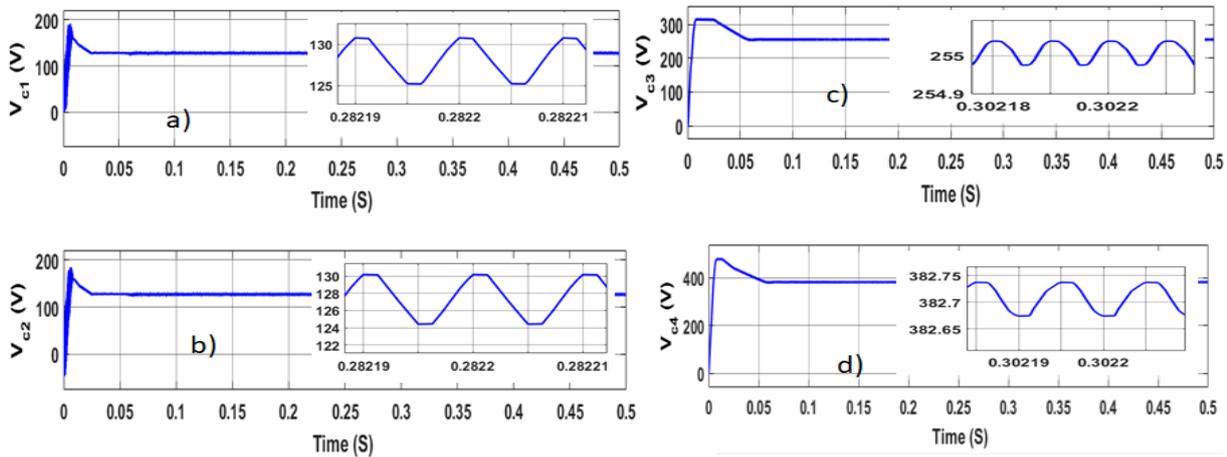


Fig. 9 Voltage across capacitor a) C<sub>1</sub> b) C<sub>2</sub> c) C<sub>3</sub> d) C<sub>4</sub>

TABLE I  
SIMULATION PARAMETER

Parameters	Specification
Input voltage ( $V_{in}$ )	48V
Output voltage ( $V_o$ )	650V
Switching frequency ( $f_s$ )	100KHz
Inductor $L_1, L_2$	600 $\mu$ H
Inductor $L_3$	1 $\mu$ H
Capacitors $C_1, C_2$	2.2 $\mu$ F
Capacitor $C_3, C_4$	100 $\mu$ F
Output capacitor $C_0$	47 $\mu$ F

### V. ANALYSIS

Analysis of DC-DC converter with voltage multiplier cell is carried out by considering parameters like voltage gain, efficiency, and duty cycle.

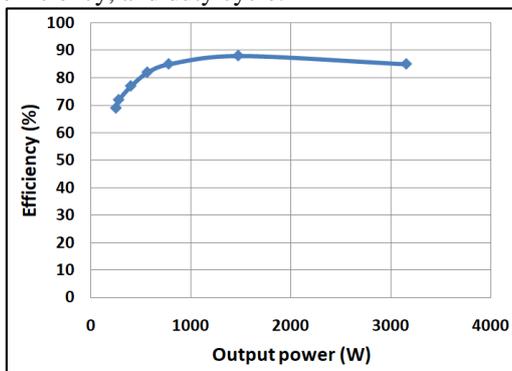


Fig. 10 Efficiency vs Output power

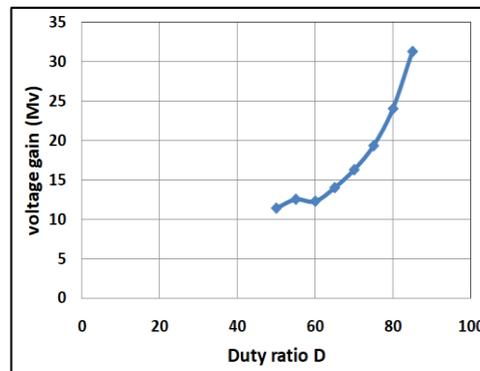


Fig. 11 Voltage gain vs Duty cycle

Fig.10 shows the efficiency curve of the converter. The efficiency increases first and then it decreases after reaching the maximum value. The maximum efficiency of the converter is around 89%. The plot of voltage gain Vs duty cycle is shown in Fig.11. The voltage gain increases with increasing duty cycle. The converter voltage gain is around 13.27. From analysis it is observed that maximum voltage gain of 34 is reached at duty cycle of 0.85.

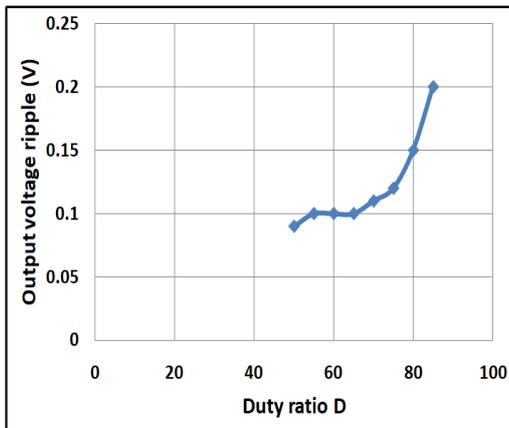


Fig. 12 Output voltage ripple vs Duty cycle

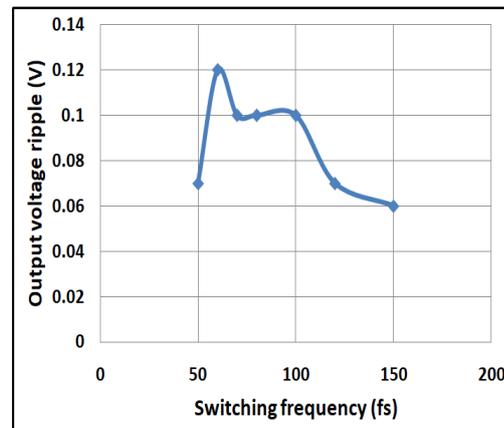


Fig. 13 Output voltage ripple vs switching frequency

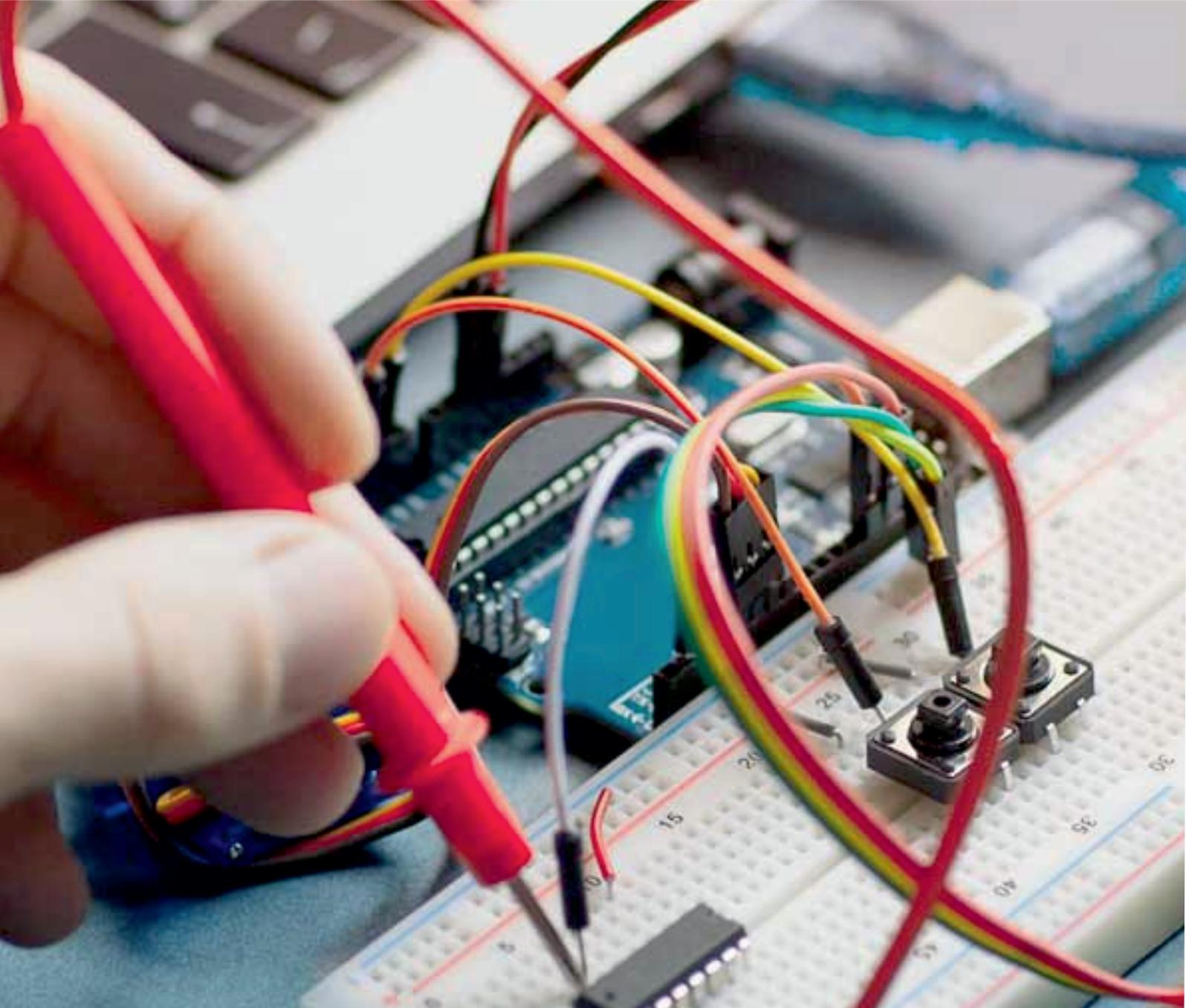
Output voltage ripple vs duty cycle is shown in Fig.12. The converter has lower output voltage ripple about 0.1 V at duty cycle of 0.631. The output voltage ripple is increases with increasing duty cycle. The plot of output voltage ripples vs switching frequency shown in Fig.13. Initially voltage ripple is increased with switching frequency and it reaches maximum at 100 kHz. Further increase of switching frequency, output voltage ripple is decreases.

## VI.CONCLUSION

The increased voltage gain is provided by the high step-up hybrid DC-DC converter. The interleaved construction contributes to decrease input current ripple, which helps renewable energy modules last longer. To boost the voltage gain, a voltage multiplier cell is utilised. The converter can be expanded on both the output and input sides, increasing the voltage gain and lowering the input current ripple. The circuit has strong expandability because it may be enlarged by adding more parallel boost channels or switched-capacitor boost units. The voltage strains on the switch and diodes are rather minimal. The large step up voltage gain is demonstrated by the input voltage of 48 V and the output voltage of 637 V. The converter has a maximum efficiency of around 89% and a voltage gain of 13.27, according to analysis. This can be utilised in renewable energy applications that require a high dc voltage, such as fuel cells and solar cells.

## REFERENCES

- [1] Lin and Zhou Zhang, "Low Input Ripple High Step-Up Extendable Hybrid DC-DC Converter", IEEE Access, October 30, 2019
- [2] Y. Jang and M. M. Jovanovi, "Interleaved boost converter with intrinsic voltage-doubler characteristic for universal-line PFC front end", IEEE Transactions on Power Electronics, vol. 22, no. 4, pp. 13941401, Jul. 2007.
- [3] K. J. Reddy and N. Sudhakar, "High voltage gain interleaved boost converter with neural network based MPPT controller for fuel cell based electric vehicle applications", IEEE Access, vol. 6, pp. 38993908, 2018.
- [4] P.Wang,L.Zhou,Y.Zhang,J.Li,andM.Sumner, "Input-parallel output series DC-DC boost converter with a wide input voltage range, for fuel cell vehicles", IEEE Transactions on Vehicular Technology, vol. 66, no. 9, pp. 77717781, Sep. 2017.
- [5] V. A. K. Prabhala, P. Fajri, "A DC-DC converter with high voltage gain and two input boost stages", IEEE Transactions on Power Electronics,.,vol.31,no.6,pp.42064215, Jun. 2016. 6792-6799, 2017.
- [6] B.Wu,S.Li,Y.Liu,andK.M.Smedley, "A new hybrid boosting converter for renewable energy applications" IEEE Transactions on Power Electronics, vol.31, no. 2, pp.12031215, Feb. 2016
- [7] A. Rajaei, R. Khazan, M. Mahmoudian, "A dual inductor high step-up DC-DC converter based on the Cockcroft Walton multiplier," IEEE Transactions on Power Electronics, vol. 33, no. 11, pp. 96999709, Nov. 2018.
- [8] G.Wu, X.Ruan,andZ.Ye, "Non isolated high step-up DC-DC converters adopting switched-capacitor cell," IEEE Transactions on Power Electronics, vol. 62, no. 1, pp. 383393, Jan. 2015.
- [9] Z.Chen,C.Zhang,Y.Wu, "Series-capacitor-based buck PFC converter with high power factor and ultrahigh step-down conversion ratio", IEEE Transactions on Industrial electronics , vol. 66, no. 9, pp. 68956905, Sep. 2019.
- [10] P. S. Shenoy, M. Amaro, J. Morroni, and D. Freeman, "Comparison of a buck converter and a series capacitor buck converter for high frequency, high-conversion-ratio voltage regulators" IEEE Transactions on Power Electronics, vol. 31, no. 10, pp. 70067015, Oct. 2016.
- [11] M.K. Nguyen, Y.C. Lim, J.H. Choi, and G.B. Cho, "Isolated high step-up DC-DC converter based on quasi-switched-boost network" IEEE Transactions on Power Electronics, vol. 28, no. 12, pp. 5758-5773, 2013



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