



# International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

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## Parametric Study of RMSA for WLAN and Wi-Max Applications

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**ABSTRACT:** The objective of this paper is to study the effect of pentagon slot on the antennas characteristics like return loss and impedance bandwidth. For this purpose a simple rectangular micro strip antenna (RMSA) is considered for ease of analysis. To start with, first a RMSA is designed and then it is modified by etching pentagon slot at various locations of the patch to study effect of it on antennas parameters.

**KEYWORDS:** Pentagon slot, return loss, impedance bandwidth, Rectangular Microstrip Antenna.

### I. INTRODUCTION

Physically, MSA consists of a metallic radiating patch backed up by a dielectric substrate and a ground plane below that. These days, MSAs are widely used in many applications due to their inherent advantages such as low profile, lightweight, planer configuration and ease of fabrication. However, main limitation of MSAs is their inherently narrow bandwidth [1]. Microstrip patch antenna can be used for multiband operation and it can be achieved by cutting various slots on the radiating patch and ground [2-4]. Optimization of the design and efficiency of printed antennas are used in communication systems [5-8]. Norbahiah Misran [2] has proposed a multi-slotted microstrip patch antenna for wireless communication system. A comparative analysis of the various geometries of MSA obtained by inserting slots on the radiating patch indicate considerable improvement in performance parameters of MSA such as return loss, radiation pattern and gain is found to be rare in the literature.

### II. ANTENNA DESIGN

The proposed antenna is designed using a low cast glass epoxy substrate material of area X x Y having a thickness  $h = 0.16$  cm with dielectric constant  $\epsilon_r = 4.2$ . The artwork of this antenna is sketched using computer software AutoCAD to achieve better accuracy.

Figure 1 (a) to (c) shows the top view geometry of the pentagon slot loaded rectangular microstrip antenna (PRMSA). The PRMSA is designed for 3.2 GHz of frequency of conventional rectangular microstrip antenna (CRMSA).

The antenna consists of a radiating patch of length L and width W. The antenna is excited through a simple microstrip line feed of length  $L_f$  and width  $W_f$ . A  $50\Omega$  semi miniature connector is used to feed the microwave power. The quarter wavelength transformer of length  $L_t$  and width  $W_t$  is used to match the impedance between  $C_p$  and microstrip line feed.

In Figure 1 (a) and (b) shows geometry of PRMSA by incorporating inverted pentagon slot with vertices V in the fourth quadrant and non inverted pentagon slot with same dimension in the first quadrant of the radiating patch respectively. Figure 1 (c) shows rectangular patch loaded with non inverted and inverted pentagon slots simultaneously.

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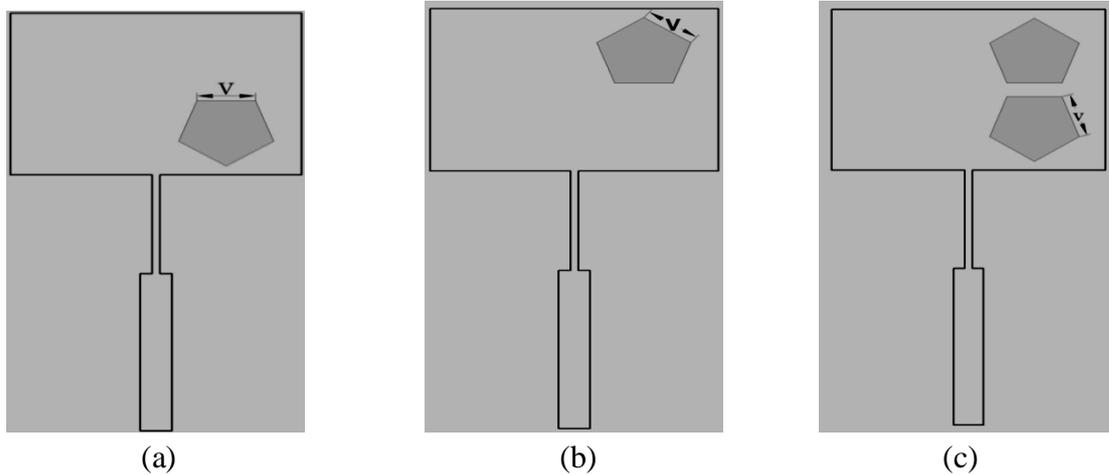


Fig. 1 Geometry of PRMSA (a) Inverted Pentagon slots in fourth quadrant, (b) Non-inverted pentagon slot in first quadrant and (c) Inverted and non inverted slots in fourth and first quadrant.

The design parameters of the proposed antenna are given in Table 1.

**Table 1** Design parameters of PSRMA

Antenna Parameters	L	W	L <sub>f</sub>	W <sub>f</sub>	L <sub>t</sub>	W <sub>t</sub>	V
Dimensions in cm	2.24	2.91	2.183	0.317	1.372	0.078	0.58

### III. EXPERIMENTAL RESULTS AND DISCUSSION

The simulation of the proposed antenna is carried out by using Ansoft electromagnetic 3D-tool. The antenna bandwidth over return loss less than -10 dB is measured experimentally by using Vector Network Analyzer (Rohde & Schwarz, Germany make ZVK model 1127.8651). The experimental bandwidth is calculated by using the formula,

$$BW = (f_H - f_L / f_r) * 100\% \quad \dots (1)$$

where  $f_H$  and  $f_L$  are upper and lower cut off frequencies respectively, when its return loss reaches 10 dB and  $f_r$  is the resonance frequency between  $f_H$  and  $f_L$ .

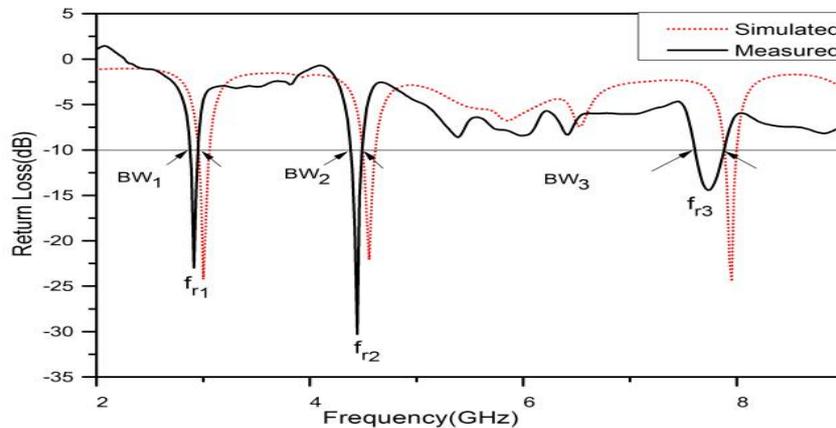


Fig. 2 Variation of frequency versus return loss of PRMSA with slot in fourth quadrant

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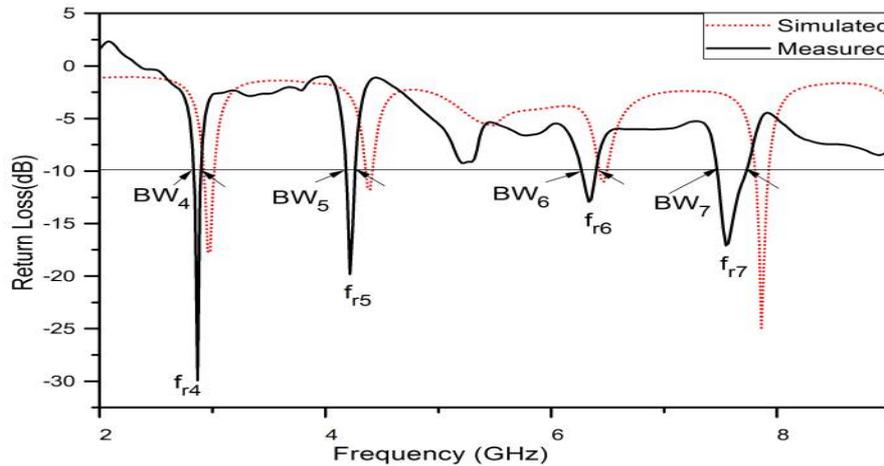


Fig. 3 Variation of frequency versus return loss of PRMSA with slot in first quadrant

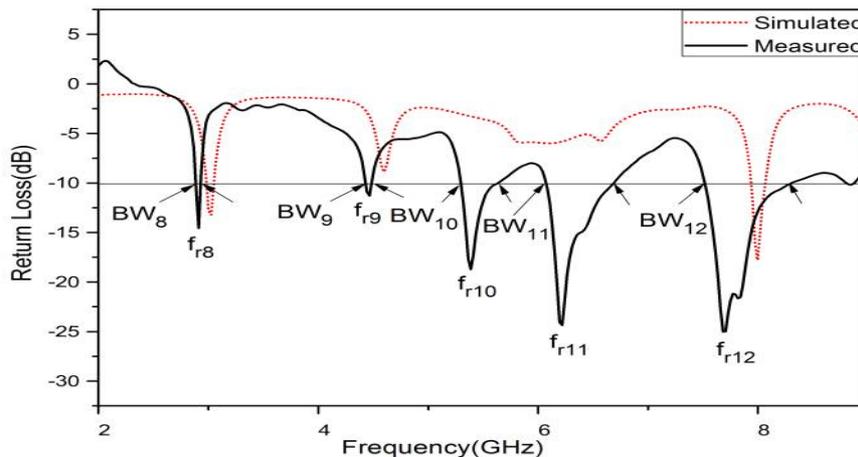


Fig. 4 Variation of frequency versus return loss of PRMSA with slot in first and fourth quadrant

The variation of return loss versus frequency of PRMSA when inverted pentagon slot is loaded in the fourth quadrant of rectangular patch is as shown in Figure 2. From this figure it is observed that, the antenna operates for triple frequency bands  $BW_1$  (3.06 – 2.93 GHz) = 4.33%,  $BW_2$  (4.61 – 4.47 GHz) = 3.07% and  $BW_3$  (8 – 7.89 GHz) = 1.38% for the resonating frequencies of  $f_{r1}$ ,  $f_{r2}$  and  $f_{r3}$  respectively. These frequency bands are due to independent resonance of the patch and pentagon slot on the radiating patch. The  $BW_1$  is considered as primary band because its resonating frequency  $f_{r1}$  is close to  $f_r$  (2.98 GHz) of CRMSA. The  $BW_2$  is considered as secondary band and  $BW_3$  as third band respectively. Further, it is seen from Figure 2 that, the simulated result of PRMSA is also shown, which is in good agreement with experimental result.

Figure 3 shows the variation of return loss versus frequency of PRMSA when non inverted pentagon slot is loaded in the first quadrant of rectangular patch. From this figure it is observed that the antenna operates for four frequency bands  $BW_4$  (2.92 – 2.80 GHz) = 4.21%,  $BW_5$  (4.26 – 4.16 GHz) = 2.36% ,  $BW_6$  (6.42 – 6.24 GHz) = 2.83% and  $BW_7$  (7.74 – 7.45 GHz) = 3.84% for the resonating frequencies of  $f_{r4}$ ,  $f_{r5}$ ,  $f_{r6}$  and  $f_{r7}$  respectively. These quad bands are obtained due to independent resonance of the patch and pentagon slot on the radiating patch. It is seen from the figure that the change in the construction of PRMSA does not affect much the primary band resonant frequency  $f_{r1}$  and secondary band resonant frequency  $f_{r2}$  of Figure 2 but introduces an additional resonating frequency  $f_{r6}$  in between  $f_{r5}$  and  $f_{r7}$ . Further, it is clear from Figure 3 that, the simulated result of PRMSA is in good agreement with experimental result.

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Figure 4 shows the variation of return loss versus frequency of PRMSA when non inverted and inverted pentagon slots are loaded in the first and fourth quadrant of rectangular patch respectively. From this figure it is observed that the antenna operates for five frequency bands  $BW_8$  (2.94 – 2.88 GHz) = 2.05%,  $BW_9$  (4.47 – 4.42 GHz) = 1.12%,  $BW_{10}$  (5.64 – 5.29 GHz) = 6.51%,  $BW_{11}$  (6.68 - 6.06 GHz) = 9.98% and  $BW_{12}$  (8.30 – 7.52 GHz) = 10.14% for the resonating frequencies of  $f_{r_8}$ ,  $f_{r_9}$ ,  $f_{r_{10}}$ ,  $f_{r_{11}}$  and  $f_{r_{12}}$  respectively. Again, it is observed from this figure that the change in construction of PRMSA does not affect much the resonant frequencies  $f_{r_1}$  and  $f_{r_2}$  of Figure 2 but introduces two additional resonant frequencies  $f_{r_{10}}$  and  $f_{r_{11}}$  in between resonant frequencies  $f_{r_9}$  and  $f_{r_{12}}$ . Further, it is clear from Figure 4 that, the simulated result of PRMSA is in good agreement with experimental result.

The gain of PRMSA is calculated using absolute gain method given by the formula [9],

$$(G)dB = 10 \log \left( \frac{P_r}{P_t} \right) - (G_t)dB - 20 \log \left( \frac{\lambda_0}{4\pi R} \right) dB \quad \dots\dots\dots(2)$$

where,  $G_t$  is the gain of the pyramidal horn antenna and  $R$  is the distance between the transmitted antenna and the antenna under test (AUT). The power received by AUT, “ $P_r$ ”, and the power transmitted by standard pyramidal horn antenna “ $P_t$ ” are measured independently. The gain measured for PRMSA is found to be 5.59 dB.

Hence by placing the pentagon slot in first, fourth and both in first & fourth quadrants of the rectangular patch the antenna is made to operate for triple, quad and penta bands.

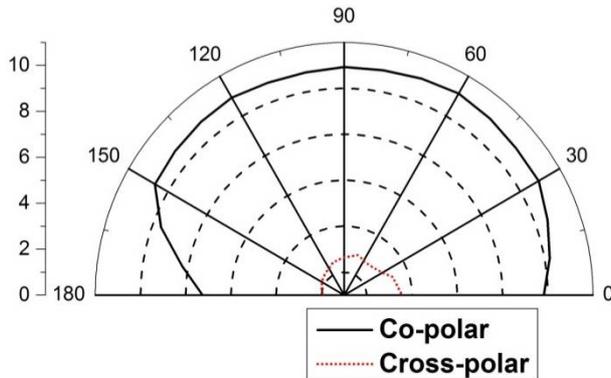


Fig. 5 (a) Radiation pattern at 3 GHz with slot in fourth quadrant

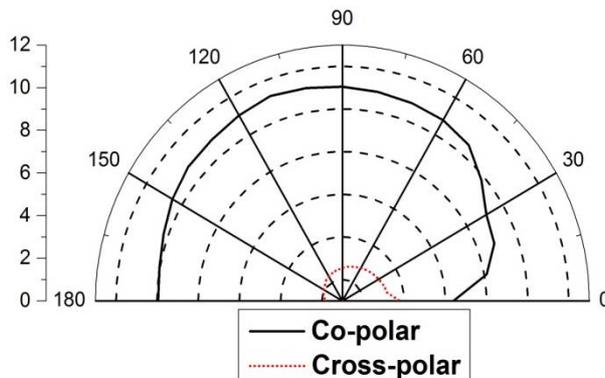


Fig. 5 (b) Radiation pattern at 2.85 GHz with slot in first quadrant

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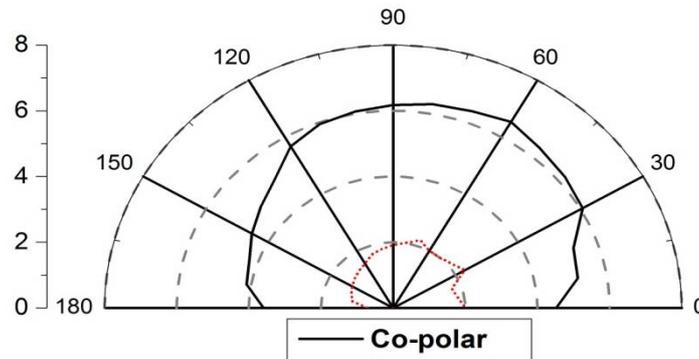


Fig. 5 (c) Radiation pattern at 2.92 GHz with slot in first and fourth quadrant

Figure 5(a) to (c) shows cross-polar and co-polar radiation patterns of PRMSA at 3 GHz, 2.85 GHz and 2.92 GHz. From the figures it is seen that radiation patterns are broadside and linearly polarized [10].

## IV. CONCLUSION

A novel design of proposed antenna is realized by CRMSA which is capable of operating for triple, quad and penta bands between 2.85 GHz to 7.95 GHz without change in linearly polarized radiation characteristics. The proposed antennas use low quality substrate material and easy to fabricate. The antenna with slots in first and fourth quadrants shows improved impedance bandwidth compared to single pentagonal slot in first and fourth quadrant separately. This antenna may find application in WLAN, Wi-MAX and fourth generation mobile communication system.

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