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Patch Antenna Parameters Variation with Ground Plane Dimensions

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ABSTRACT: An inset fed rectangular patch antenna is designed to operate at 2.4 GHz using an FR-4 substrate of height h=1.6mm. Initially the ground plane dimensions are kept as 6h+L and 6h+W (short edge); Where L is length of patch and W is width of patch. It is found to have a low gain. To improve the gain, ground plane dimensions length and width are varied in multiples of Length (L) and Width (W) respectively. For double ground (2L, 2W) case, a gain of 2.6494dB is observed. A further improved gain of 3.0524dB is achieved by using triple ground (3L, 3W).The other parameters like VSWR, Return Loss and directivity are also improved by increasing ground plane dimensions .The antennae are fabricated and tested using VNA E5071C.

KEYWORDS: Gain, Return Loss, VSWR and Directivity.

I.INTRODUCTION

Patch antennas have become popular in the recent days due to various advantages like their low profile, low cost, compatibility with IC technology and conformability with any shaped surface [1]. Recent technology advancements necessitate antenna design to wide band performance.

Patch antennas come in different shapes, but most commonly used shapes are rectangular and circular. The dimensions of patch antenna depend on the operating frequency and the dielectric constant of the substrate. The higher the operating frequency, the lower is the size of the patch [3].

The paper focuses on design, simulation, fabrication and analysis of a patch antenna operating at 2.4GHz with varying ground plane dimensions. It is observed that increased dimensions of ground plane increases the gain of the antenna. Other parameters measured are Return Loss and VSWR.

II. ANTENNA DESIGN

Configuration of the patch antenna is shown in Figure 1



Figure 1: Geometry of the patch antenna

The patch antenna dimensions are designed on the basis of transmission line model [1].



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Step 1: Selection of f_0 , ε_r , h:

- Resonant frequency selected(f_0) :2.4GHz
- Dielectric constant(ε_r) :4.4
- Height(h) :1.6mm

Step 2: Calculation of Width (*W*):

$$W = \frac{C}{2f_0\sqrt{(\varepsilon_r + 1/2)}}$$

Where $C = 3*10^8 \text{m/s}$

Step 3: Calculation of Actual Length (L):

The effective length of patch antenna depends on the resonant frequency (f_0) .

$$L_{eff} = \frac{c}{2f_0\sqrt{\varepsilon_{reff}}}$$

Where $\varepsilon_{reff} = \frac{\varepsilon_r + 1}{2} + \frac{\varepsilon_r - 1}{2} \left[1 + 12 \frac{h}{W} \right]^{-\frac{1}{2}}$

The effective length of patch antenna is equal to the one half of a wave length within the dielectric medium.

The E-fields at the edges of the patch undergo fringing effects. Because of these effects, effective length of the patch antenna appears to be greater than its actual length. So, actual length of the patch antenna is usually considered as $L < \frac{\lambda}{2}$.

Actual length and effective length of a patch antenna can be related as

$$L = L_{eff} - 2\Delta L$$

Where ΔL is a function of effective dielectric constant ε_{reff} and the width to height ratio $\left(\frac{W}{h}\right)$.

$$\frac{\Delta L}{h} = 0.412 \frac{(\varepsilon_{reff} + 0.3) \left(\frac{W}{h} + 0.264\right)}{(\varepsilon_{reff} - 0.258) \left(\frac{W}{h} + 0.8\right)}$$

Step 4: Calculation of Inset feed Depth (y_0) :

The edge of the patch antenna will have high input impedance. Impedance falls rapidly if the inset position is moved from edge of the patch towards the centre .For providing impedance matching with a 50 Ω connector, a curve fit formula for the inset feed depth y_0 is expressed as [2]

$$y_0 = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^4 - 682.69\varepsilon_r^3 + 2.561.9\varepsilon_r^2 - 4043\varepsilon_r + 6697 \} \frac{L}{2} = 10^{-4} \{ 0.016922\varepsilon_r^7 + 0.13761\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 93.187\varepsilon_r^6 - 6.1783\varepsilon_r^5 + 6.561\varepsilon_r^6 - 6.1783\varepsilon_r^6 - 6.1780\varepsilon_r^6 - 6.1$$

Step 5: Calculation of feed width (W_f) :

To achieve 50 Ω characteristic impedance, the required feed width to height ratio $\left(\frac{W_f}{h}\right)$ is computed as [1]



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$$\frac{W_f}{h} = \begin{cases} \frac{8e^A}{e^{2A} - 2} \frac{W_0}{h} \le 2\\ \frac{2}{\pi} \left\{ B - 1 - \ln(2B - 1) + \frac{\varepsilon_r - 1}{2\varepsilon_r} \left[\ln(B - 1) + 0.39 - \frac{0.61}{\varepsilon_r} \right] \right\} \frac{W_0}{h} \ge 2 \end{cases}$$

.Where

Step 6: Calculation of notch gap (*g*):

 $A = \frac{Z_0}{60} \sqrt{\frac{\varepsilon_r + 1}{2}} + \frac{\varepsilon_r + 1}{\varepsilon_r - 1} \left(0.23 + \frac{0.11}{\varepsilon_r} \right)$

Resonant frequency of patch antenna depends on the notch gap (g). Expression which relates notch gap and resonant frequency is given by [5]

$$g = \frac{v_0}{\sqrt{2 * \varepsilon_{reff}}} \frac{4.65 * 10^{-12}}{f_0(in \, GHz)}$$

With the help of above equations the dimensions of the patch are calculated and shown in Table I.

Description	Value (mm)		
Width of the Patch(W)	38.036		
Length of Patch(L)	29.443		
Width of Microstrip feed(W_f)	3.059		
Notch gap (g)	0.2		
Inset feed depth(y_0)	9.044		

TABLE I Dimensions of the patch antenna

 $B = \frac{377\pi}{2Z_0\sqrt{\varepsilon_r}}$

III.RESULTS AND DISCUSSION

By considering the ground plane dimensions i.e., Length and Width of substrate as 6h+L and 6h+W (short edge), along with the dimensions in Table Ia patch antenna is drawn. It is simulated using HFSS 13.0and fabricated by thermo lithography. Patch is tested using VNA E5071C.It is found that the patch resonates at 2.35GHz with reflection coefficient -10.2411dB. At 2.4GHz, Reflection coefficient observed is-5.8404 dB. From this it is observed that frequency of resonance is at 2.35GHz instead of 2.4GHz. To achieve the frequency of resonance at 2.4GHz,only notch gap is varied and all other dimensions are kept constant. At notch gap=0.6mm, reflection coefficient observed is-8.6242dB at 2.4 GHz.

Generally for antenna to radiate efficiently reflection co-efficient should be less than -9.5424dB. To improve the reflection co-efficient, length of the patch is varied by keeping notch gap (g) =0.6mm. Now the dimensions of the inset fed short edge patch antenna are considered as in Table II to resonate at 2.4GHz.Figure 2(a) shows the top view of the patch and Figure 2(b) shows the bottom view of the patch.Simulated reflection co-efficient curve (S_{11}) and VSWR for the inset fed short edge patch antenna in HFSS 13.0 is shown in Figure 3 and Figure 4 respectively.



Dimensions of the inset fed short edge patch antenna

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Description	Value (mm)
Width of the Patch(W)	38.036
Length of Patch(L)	28.9
Width of Microstrip feed(W_f)	3.059
Notch gap (g)	0.6
Inset feed depth(y_0)	9.044

Figure 2(a): Top view of an inset fed short edge patch antenna

Figure 2(b): Bottom view of an inset fed short edge patchantenna



Figure 3: Reflection co efficient (s_{11}) in dBCurve for inset fed short edge patch antenna with ground plane dimensions 6h+L and 6h+W

TABLE II



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Figure 4: VSWR Curve for inset fed short edge patch antenna with ground plane dimensions 6h+L and 6h+W

From Figure 3 and Figure 4 it is observed that reflection co-efficient (s_{11}) and VSWR are -13.1508 dB, 1.5642 respectively at 2.4GHz

By considering the above dimensions in Table II the patch is fabricated and tested by using VNA E5071C. Fabricated patch is shown in Figure 5.



Figure 5: Fabricated inset fed short edge patch antenna with ground plane dimensions 6h+L and 6h+W

The reflection co-efficient s_{11} in *dB* for the Inset fed short edge patch is shown in Figure 6 and Figure 7 shows the VSWR curve of the fabricated inset fed patch antenna.



Figure 6: Reflection co efficient $(s_{11}in \, dB)$ curve of the fabricated inset fed short edge patch antenna with ground plane dimensions 6h+L and 6h+W



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Figure 7: VSWR curve of the fabricated inset fed short edge patch antenna with ground plane dimensions 6h+L and 6h+W

From Figure 6 and 7 the reflection co efficient ($s_{11}in dB$) and VSWR of the fabricated inset fed Short edge patch antenna are observed as-12.172dBand 1.6233 respectively at 2.4053367GHz



Gain of an inset fed short edge patch antenna is shown in Figure 8.

Figure 8: Gain plot of the inset fed short edge patch antenna with ground plane dimensions 6h+L and 6h+W From Figure 8 the gain of the patch is noticed to be only 1.5948dB at 2.4 GHz.



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To improve the gain, ground plane dimensions are varied as doubleground (2L, 2W) and triple ground (3L, 3W). Along with gain other parameters Reflection coefficient, VSWR and directivity are observed. The simulated results using HFSS 13.0 and the measured values using VNA E5071C are kept in Table III.

Ground plane dimensio	Resonant Frequency in GHz		Reflection coefficient (S11) in dB		VSWR		Gain in dB	Directi vity in dB
-115	Simulated	Measured	Simulated	Measured	Simulated	Measured	Simulated	Simulated
Short Edge (6h+L, 6h+w)	2.4	2.405336	-13.1508	-12.172	1.5642	1.6233	1.5948	4.8816
Double Ground (2L,2W)	2.4	2.407878	-18.5306	-19.750	1.2162	1.2344	2.6495	5.7486
Triple Ground (3L,3W)	2.4	2.407878	-20.2146	-25.705	1.2687	1.0797	3.0524	6.6480

TABLE III	COMPARISON OF PARAMETERS FOR GROUND PLANE VARIATIONS

VI.CONCLUSION

By varying ground plane dimensions from short edge (6h+L, 6h+w) to triple ground (3L, 3W) there is an improvement in Return Loss from -13.15 dB to -20.2146 dB at 2.4 GHz and also a gain improvement from 1.5948dB to 3.0524dB is observed. This confirms that the design of ground plane with suitable dimensions along with the patch design is important for optimization of parameters.

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