



Design of Hybrid Coupler

T.Jayachitra, V.K Pandey and Anshuman Singh,

Noida Institute of Engineering and Technology, Greater Noida, UP, India

ABSTRACT: Hybrid couplers are widely used in microwave circuit design. The principle of a hybrid coupler is that the input power is split equally between the coupled and through ports, with a 90 degree phase difference. The fourth (isolated) port is terminated by a 50-ohm load. Hybrid coupler can be directly connected to microstrip antenna to get circular polarization. Microstrip patch antennas being popular because of light weight, low volume, thin profile configuration which can be made conformal. Wireless communication systems applications circular polarization antenna is placing vital role. In this study the hybrid coupler is designed for 2.4GHz with impedance (Z_0) is 50Ω , dielectric constant ϵ_r is 4.6 and thickness of dielectric material is 1.6mm. Simulation is done by ADS software.

Index Terms—Hybrid Coupler, Microstrip antenna, Polarization, Quadrature hybrid, 3 dB hybrid coupler.

I. INTRODUCTION

In power divider, hybrid is a special case where the signals at the two output ports are equal and differ in phase by 90 degree. They are used in amplifier systems where solid state power is insufficient during individual amplifier limitations, power enhanced by using multiple amplifiers in a hybrid network. By choosing appropriate capacitance the circuit can act as a quadrature amplitude-tunable power splitter [1] and by cascading hybrids in a tree/ a matrix divider/combiner configuration, more power is transmitted, as well as improving the efficiency of the transmission [2]. The types of power divider are as follows.

The Quadrature Hybrid

The quadrature hybrid is shown in Figure 1a. It is a four-port network, the input is at port 1 and the output ports 2 and 3, when port 4 is terminated in a match load. Alternatively, port 4 is the input and port 1 match – terminated when the output remains at ports 2 and 3. The operation of the hybrid is not affected when ports 1 and 4 are interchanged with ports 2 and 3 because of a high degree of symmetry [3].

Ports 1 and 4 or vice versa are assigned with the input based on the required logic of circular polarization. Meanwhile, ports 2 and 3 are provided for the output.

However, the signal is split into amplitude; ports 2 and 3 are allocated with in phase quadrature. Inconsistency might happen at port 4 due to the patch returns to the absorbing load. Port 2 and 3 are uncoupled, good isolate, and surpassing 20 dB exists between the outputs. Therefore, the axial is not degraded. Four port direct coupled power divider is used for designing a 3-dB quadrature hybrid. The characteristic impedances Z_a and Z_b of a quarter-guide wave length shunt and series arms are obtained in terms of $Z_b - Z_0/\sqrt{2}$ and $Z_a - Z_0$.

3 dB, 90 degree hybrids are recognized as construction hybrids. As a result, sign is applied to any input to divide it into two equal amplitude signals rather than 90 degree. It won't create any difference since the outputs remains as similar as these devices square measure electrically and mechanically balanced. This relationship ensures a high degree of isolation between the two output ports and therefore the two input ports do not need interaction between them.

The 180-Degree Ring Hybrid

The ring hybrid is a 180-degree hybrid junction, as shown in Figure 1b. The input given at Port 1 is

equally divided into amplitude and phase and applied at ports 2 and 3 which are all linked with the patch dual-orthogonal feeds. A quadrature phase difference among the two orthogonal excitations can be attained using a quadrature wave length differential line length between the two outputs lined. Due to the 90 degree phase shift between the output arms, at port 1 the reflection from the patch is getting cancelled. Therefore ports 2 and 3 are uncoupled and the outputs are having good isolation. It is usually better than 20dB. The sense of circular polarization rotation can be changed, if port 4 becomes the input and port 1 is match-terminated while keeping everything else the same. The line parameters can be obtained from the general design equations of a hybrid-ring coupler. For a 3-dB split, the characteristic impedance of the ring Z_b is found to be Z_0 [3].

Wilkinson power divider

Figure 1c represents that, the input at port 1 consistently characterized according to the amplitude and phase at output ports 2 and 3. According to the ring hybrid, the dual feeds can be recognized by quarter wavelength line among output ports 2 and 3 at the level of 90 degree phase. Therefore, the result placed among any two level output ports at 90 degree phase while it finds any reflection at the patch as odd mode excitation can degenerate in the isolation resistor.

But, the antenna reliability will be decrease while maintaining good matching [3].

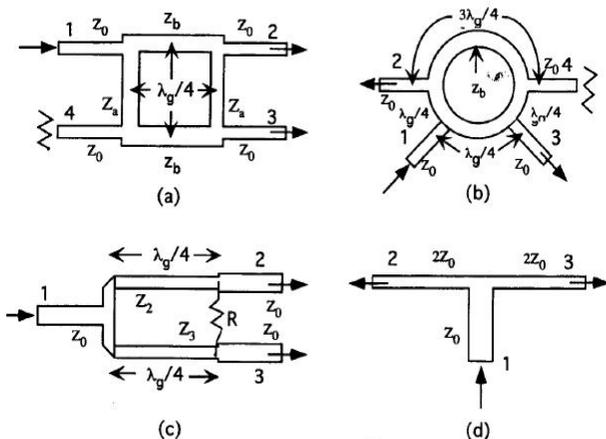


Fig.1 (a) Quadrature Hybrid, (b) ring hybrid, (c) Wilkinson power divider, (d) T-Junction power divider.

3 dB Quadrature Hybrid Coupler

A 3 dB, 90° hybrid coupler is a four-port device, that is used either to equally split an input signal with a resultant 90° phase shift between output signals or to combine two signals while maintaining high isolation between them. However, in a practical device the amplitude balance is frequency dependent and departs from the ideal 0dB difference. All 90° Power Dividers/Combiners, also known as quadrature hybrids or simply quad hybrids, are reciprocal four port networks . Figure 2 is a functional block diagram of a 3 dB quad hybrid coupler. The hybrid coupler, or 3 dB directional coupler, in which the two outputs are of equal amplitude, takes many forms. It is beginning when quadrature (90 degree) 3 dB coupler coupling with outputs 90 degrees out of phased. Now any matched 4-port with isolated arms and equal power division is called a hybrid or hybrid coupler. Now a days the characterizing feature is the phase difference of the outputs In an ideal hybrid circuit, the difference should be 0 dB.

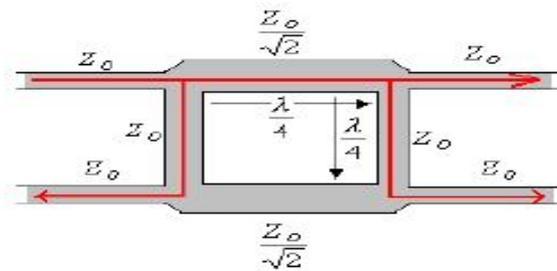


Fig.2 3dB Hybrid coupler

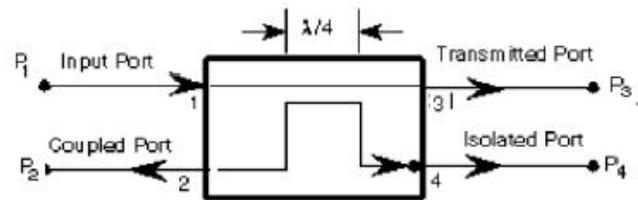


Fig.3 Internal diagram of 3dB quad hybrid coupler

Referring to Figure 3, a signal applied to port 1 splits equally between ports 2 and 3 with one of the outputs exhibiting a relative 90° phase shift. If ports 2 and 3 are properly terminated into matching impedances, nearly all

the signal applied to port 1 is transmitted to the loads connected to ports 2 and 3. In this circumstance, port 4 receives negligible power and is termed as isolated. However, if there is an impedance mismatch at port 2, for example, then signal power reflected back from port 2 were divided proportionally between ports 1 and 4 and power is not fed to port 3. In this paper, design of 3 dB 90 degree hybrid coupler is done.

II. DESIGN OF HYBRID COUPLER

Thickness of the Substrate is taken as 1.6 mm and dielectric constant 4.6. Operating frequency has chosen as 2.4Ghz. The design of Hybrid coupler is as follows

$$\frac{w}{d} = \frac{8e^A}{e^{2A-2}} \quad \text{for } \frac{w}{d} < 2 \quad (3)$$

$$\frac{w}{d} = \frac{2}{\pi} \left[\frac{B-1-\ln(2B-1)}{2\epsilon_r} + \frac{\epsilon_r-1}{2\epsilon_r} \left\{ \ln(B-1) + 0.39 - \frac{0.61}{\epsilon_r} \right\} \right] \quad \text{for } \frac{w}{d} > 2 \quad (4)$$

Consider $\frac{w}{d} > 2$

$$B = \frac{377\pi}{2z_0\sqrt{\epsilon_r}} \quad (5)$$

Given $z_0 = 50\Omega$ $\epsilon_r = 4.6$ h or $d = 1.6\text{mm}$

$$B = \frac{377\pi}{2 \times 50 \times \sqrt{4.6}} = \frac{1183.78}{214.476}$$

$$B = 5.52$$

$$\frac{w}{d} = \frac{2}{\pi} \left[\frac{B-1-\ln(2B-1)}{2\epsilon_r} + \frac{\epsilon_r-1}{2\epsilon_r} \left\{ \ln(B-1) + 0.39 - \frac{0.61}{\epsilon_r} \right\} \right] \quad (6)$$

$$= \frac{2}{3.14} \left[\frac{5.519-1-\ln(2 \times 5.519-1)}{2 \times 4.6} + \frac{4.6-1}{2 \times 4.6} \left\{ \ln(5.519-1) + 0.39 - \frac{0.61}{4.6} \right\} \right]$$

$$= \frac{2}{3.14} [2.213 + 0.6905]$$

$$\frac{w}{d} = 1.8492$$

$$w = 2.95\text{mm}$$

Length of the hybrid (l):

$$l = \frac{90^\circ (\pi \times 180^\circ)}{\sqrt{\epsilon_e} \times k_0} \quad (7)$$

$$k_0 = \frac{2\pi f}{c} = \frac{2\pi \times 2.4 \times 10^9}{3 \times 10^8}$$

$$k_0 = 50.24$$

$$l = \frac{90^\circ (\pi \times 180^\circ)}{\sqrt{3.457} \times 50.24}$$

$$l = 16.81\text{mm}$$

Effective Dielectric constant (ϵ_e):

$$\epsilon_e = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \sqrt{1 + \frac{12d}{w}} \quad (8)$$

$$= \frac{4.6 + 1}{2} + \frac{4.6 - 1}{2} \frac{1}{\sqrt{1 + \frac{12 \times 1.6 \times 10^{-3}}{2.958 \times 10^{-2}}}}$$

$$= 2.8 + 1.8(0.3653)$$

$$\epsilon_e = 3.45$$

III. RESULTS AND DISCUSSION

The simulation of 3 dB hybrid coupler is done on ADS software and we get simulation results of return loss, Gain, 3D E- fields. Figure 5 depicts the resonating frequency of proposed hybrid coupler is 2.4 GHz and the return loss is -31.905dB. This low value of return loss yields higher efficiency in WLAN applications. Figure 4,5 shows the layout and photograph of a hybrid coupler on FR4 PCB . Figure 6 and 7 shows the return loss characteristic of simulated and fabricated antenna, both are in a good agreement. Figure 8 shows the 3D radiation pattern and Figure 9 shows the gain and directivity of the hybrid coupler. The simulated and measured results satisfy the requirements of wireless communication.

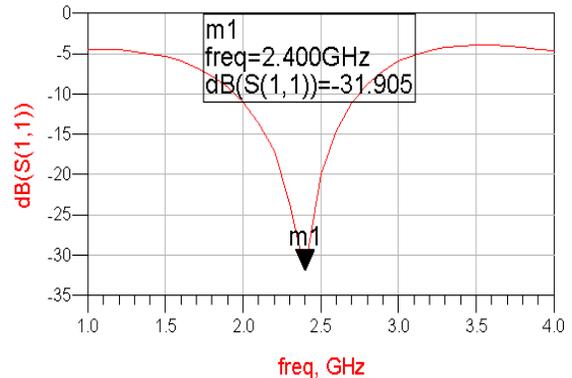


Fig.6 Simulated result of Return loss Characteristic

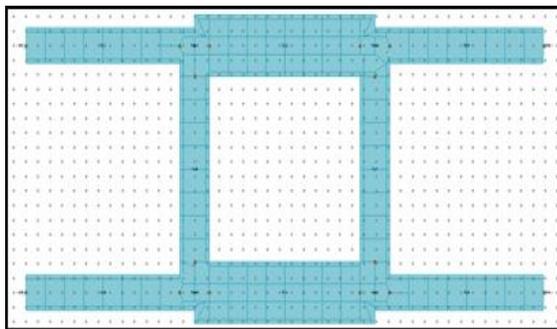


Fig.4 Proposed Antenna Layout design in ADS



Fig.7 Measured result of return loss Characteristic



Fig.5 Photograph of a hybrid coupler with FR4 dielectric

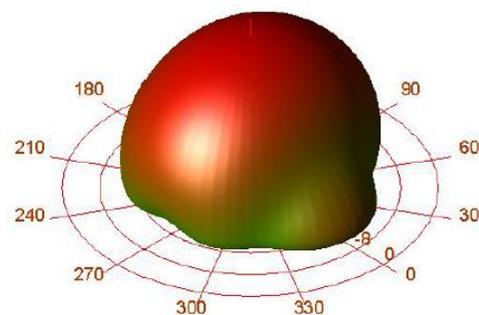


Fig.8 3D Radiation Pattern of Hybrid coupler



Fig.9 Gain and Directivity of Proposed Hybrid Coupler

TABLE I
HYBRID COUPLER RESULTS

Specifications	Observation
Frequency(GHz)	2.404
Return Loss (dB)	-30
Power radiated(W)	15.2×10^4
Effective angle	3.24
Gain	-4.37
Directivity	5.87
Efficiency	55%
Maximum intensity	4.68×10^4
HPBW(dB)	85.1496

IV. CONCLUSION

In this paper, 3 dB hybrid coupler was chosen. The hybrid coupler is designed to operate at 2.404 GHz frequency. The hybrid coupler is successfully implemented and fabricated. The performance of the simulated and fabricated hybrid coupler agreed well. The 3 dB hybrid coupler can be connected with patch antenna to produce circular polarization.

REFERENCES

- [1] Park J.-I and Kim C.-S. (1999), "Modeling of a photonic bandgap and its application for the low-pass filter design," Asia Pacific Microwave Conf. Proc. APMC, Vol. 2, 331–334.
- [2] Pozar D.M. (2005), "Microwave Engineering", Third Edition, John Wiley & Sons.
- [3] De Ronde F.C. (1970), "A new class of microstrip directional coupler", IEEE Int. Microwave Symp. Dig., pp.184 -189.
- [4] Takimoto, Y., Recent activities on millimeter wave indoor LAN system development in Japan," Dig. IEEE Microwave Theory and Techniques Society Int. Symp., 405{408, Jun. 1995.
- [5] Huang, J., "Planar microstrip Yagi array antenna," IEEE Antennas and Propagation Society Int. Symp., Vol. 2, 894{897, Jun.1989}.

- [6] Pramendra Tilanthe, P. C. Sharma, and T. K. Bandopadhyay, "Gain Enhancement of Circular Microstrip Antenna for Personal Communication Systems," IACSIT International Journal of Engineering and Technology, Vol.3, No.2, April 2011.
- [7] J. -Y. Park, C. Caloz, Y. Qian, and T. Itoh, "A compact circularly polarized subdivided microstrip patch antenna," IEEE Microwave Wireless Component Letters, vol. 12, pp. 18-19, Jan 2002.
- [8] S. Zhang, C. Zhu, J. K. O. Sin, and P. K. T. Mok, "A novel ultrathin elevated channel low-temperature poly-Si TFT," IEEE Electron Device Lett., vol. 20, pp. 569–571, Nov. 1999.
- [9] D. A. El Aziz and R. Hamad, "Wideband Circular Microstrip Antenna For Wireless Communication Systems," Radio Science Conference, pp. 1-8, March 2007.
- [10] Jagdish. M. Rathod, "Comparative Study of Microstrip Patch Antenna for Wireless Communication Application", International Journal of Innovation, Management and Technology, Vol. 1, No. 2, June 2010
- [11] RSA Raja Abdullah, D Yoharaaj , "Bandwidth Enhancement for Microstrip Antenna in Wireless Applications", Modern Applied Science, Vol.2, No.6, Nov 2008.
- [12] Haskins,P. M. and J. S. Dahele,"Varactor-diode loaded passive polarisation-agile patch antenna," Electronics Letters,Vol. 30, 1074–1075,June 1994.
- [13] Ho,M. H.,M. T. Wu,C. G. Hsu,and J. Y. Sze,"An RHCP/LHCP switchable slotline-fed slot-ring antenna," Microwave and Optical Technology Letters,Vol. 46,30–33,2005.
- [14] Jieh-Sen Kuo and Gui-Bin Hsieh, "Gain Enhancement of a Circularly Polarized Equilateral-Triangular Microstrip Antenna with a Slotted Ground Plane," IEEE Transactions on Antennas and Propagation, vol. 51, no. 7, July 2003.
- [15] Ferrero F., Luxey C., Jacquemod G., and Staraj R., Dual-Band Circularly Polarized Microstrip Antenna for Satellite Application, IEEE Antennas and Wireless Propagation Letters, vol. 4, pp. 13-15, 2005.
- [16] B. Lindmark, "A novel dual polarized aperture coupled patch element with a single layer feed network and high isolation," in Proc. IEEE Antennas and Propagation Soc. Int. Symp. Dig., vol. 4, 1997, pp. 2190–2193.
- [17] D. K. Paul, P. Gardner, "Microwave quadrature active phase shifter using Mesfets," Microwave & Optical Tech. Lett., vol. 15, pp. 359-360, Aug. 1997.
- [18] C. Luxey and J.-M. Laheurte, "Dual-beam array of microstrip leaky-wave antennas," Electronics Lett., vol. 34, no. 11, pp. 1041-1042, 28th May 1998.
- [19] B. Lindmark, "A novel dual polarized aperture coupled patch element with a single layer feed network and high isolation," in Proc. IEEE Antennas and Propagation Soc. Int. Symp. Dig., vol. 4, 1997, pp. 2190–2193.