



Analysis of IM Fed by Multi-Carrier SPWM and Low Switching Frequency Mixed CMLI

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ABSTRACT: This paper presents analysis of induction motor fed by a Multi-carrier based sinusoidal pulse width modulation (SPWM) and a low frequency switching mixed cascaded multilevel inverter (MCMLI). A cascaded multilevel inverter using a single dc source and a capacitor is promising quality output waveform is known as mixed cascaded multilevel inverter (MCMLI) and its implementing with seven-level. Since the method using low frequency switching it has less switching losses and has high single stage output efficiency. Also the paper presents modelling and simulation of a Multi-carrier based SPWM Multilevel Inverter of high switching frequency, thereby showing the output comparison to MCMLI. Both test systems are modelled using MATLAB. In this work, SIMULINK is used and tested Induction Motor characteristics at different loads.

Keywords: Multi Level Inverter (MLI), Mixed Cascaded Multi Level Inverter (MCMLI), Total Harmonic Distortion (THD), Sinusoidal Pulse Width Modulation (SPWM), Induction Motor (IM).

I. INTRODUCTION

The Multilevel converters are mainly use to synthesize a designing of an single- or three-phase voltage waveform, many topologies are introduced in multilevel inverters like diode-clamped method, flying back capacitor, and cascaded structures method, are intensively studied for high-power applications because of its low electromagnetic interference and high efficiency, as in [1]-[6]. These inverters can solve the problems associated with existing 2-level inverters. Solar cells, fuel cells, batteries, and ultra-capacitor are the most common used independent sources, as in [3]. This structure can be considered in two arrangements, symmetrical and asymmetrical. The use of asymmetric input voltages can reduce, or when properly chosen, eliminate redundant output levels. In addition more different output voltage levels can be generated with the same number of components, compared to a symmetric multilevel inverter.

Traditionally, in each phase of a cascaded multilevel inverter requires n number of dc sources for $2n + 1$ level. For many applications, obtaining so many separate dc sources may preclude the use of an inverter, as in [9]. The control aim of the MCMLI needs to maintain the balance of the dc voltage level of the capacitors while producing a nearly sinusoidal three-phase output voltage using a low frequency switching harmonic elimination method. This paper utilizing a method called the seven-level fundamental frequency harmonic elimination method to MCMLI.

II. PRINCIPLE OF HCMLI

To operate a cascaded multilevel inverter using a single dc source, capacitors are used as the dc sources for all but the first source. To explain, consider a cascaded multilevel inverter with two blocks as shown in Fig. 1. The dc source for the first block is a battery or fuel cell with an output voltage of V_{dc} , while the dc source for the second block (H_2) is a capacitor whose voltage is to be held at V_c . The output voltage of the first block is denoted by V_1 and the output of the second block is denoted by V_2 so that the output voltage of the cascaded multilevel inverter is

$$V(t) = V_1(t) + V_2(t)$$

By opening and closing the switches of H_1 appropriately, the output voltage V_1 can be made equal to $-V_{dc}$, 0, or V_{dc} , while similarly the output voltage of H_2 can be made equal to $-V_c$, 0, or V_c by opening and closing its switches

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appropriately. Therefore, the output voltage of the inverter can have the values $-(V_{dc} + V_c)$, $-V_{dc}$, $-(V_{dc} - V_c)$, $-V_c$, 0 , V_c , $(V_{dc} - V_c)$, V_{dc} , and $(V_{dc} + V_c)$, which constitute nine possible output levels, as in [9].

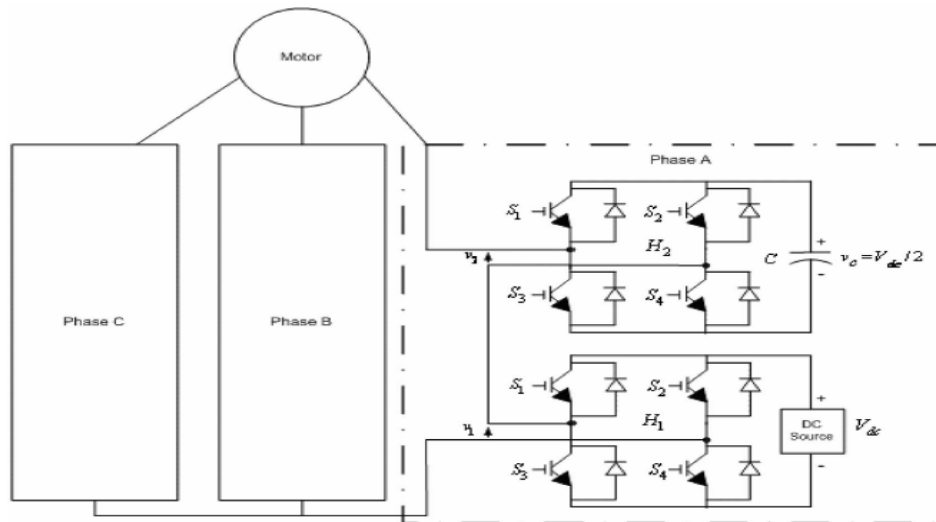


Fig.1 Topology of the proposed multilevel inverter with a single dc source -Three-phase topology

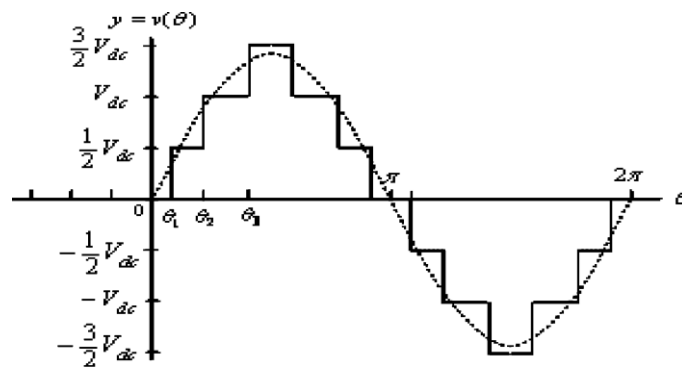


Fig.2 Seven-level equal step output-voltage waveform

To balance the capacitor's voltage, not all the possible voltage levels must be used in a cycle. A simple seven-level output voltage case $-3V_{dc}/2$, $-V_{dc}$, $-V_{dc}/2$, 0 , $V_{dc}/2$, V_{dc} , $3V_{dc}/2$ can be designed, as shown in Fig. 2, when the capacitor block voltage V_2 and dc source block voltage V_1 are cascaded as shown in Fig. 3.

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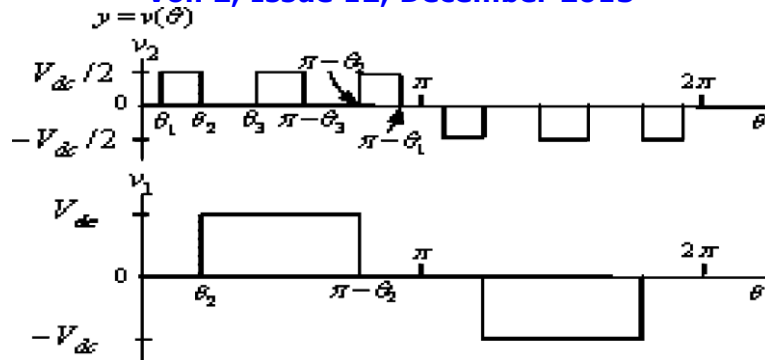


Fig.3 H-bridge voltages V_1 and V_2 control for $\theta_1 \leq \theta < \theta_2$, $V_1 = 0$ and $V_2 = V_{dc} / 2$

The Fourier series expansion of the seven-level equal step output voltage waveform shown in Fig. 2 is

$$V(\omega t) = \sum_{n=1,3,5,\dots}^{\infty} \frac{2V_{dc}}{n\pi} (\cos(n\theta_1) + \cos(n\theta_2) + \cos(n\theta_3)) \sin n\omega t \dots \text{Eqn. (1)}$$

Where n is the harmonic number of the output voltage of the multilevel inverter. Ideally, required fundamental component V_1 . For three-phase inverter applications, the triplen harmonics in each phase need not be cancelled as they automatically cancel in the line-to-line voltages. The goal is to achieve the fundamental and eliminate the fifth and seventh harmonics. Using Eqn. (1), this can be formulated as the solution to the following equations:

$$\begin{aligned} \cos \theta_1 + \cos \theta_2 + \cos \theta_3 &= m \\ \cos 5\theta_1 + \cos 5\theta_2 + \cos 5\theta_3 &= 0 \\ \cos 7\theta_1 + \cos 7\theta_2 + \cos 7\theta_3 &= 0 \dots (2) \end{aligned}$$

Switching Angle Solution:

Eliminating the third, fifth and seventh harmonics and achieving required fundamental component V_1 is done by calculating firing angles $\theta_1, \theta_2, \theta_3$ with the solution of Eqn. (2) and these angles lines between 0 to $\pi/2$. Transcendental equations Eqn. (2) is converted into polynomials equations then solution of these polynomials gives the switching angle solution, is known as resultant theory. Since the output voltage follows the one fourth symmetry, other firing angles can be calculated with advancement of angle $\pi/2$ and similarly after π to 2π .

III. MULTI-CARRIER BASED SPWM

There are two PWM methods mainly used in multilevel inverter control strategy. One is fundamental switching frequency and another one is high switching frequency. The MCMLI explained comes under fundamental switching frequency control strategy. In high switching frequency control among the available methods SPWM is the most used for the multilevel inverter, because it is very simple and easy to implement.

This work is done utilizing the simplicity of multi carrier sine PWM. For an n -level inverter, $n-1$ carriers with the same frequency f_c and the same amplitude A_c are disposed such that the bands they occupy are contiguous. The reference waveform has maximum amplitude A_m , a frequency f_m , and its zero centered in the middle of the carrier set. The reference is continuously compared with each of the carrier signals. If the reference is greater than a carrier signal, then the GTO corresponding to that carrier is switched on and if the reference is less than a carrier signal, then the GTO corresponding to that carrier is switched off.

In multilevel inverters, the amplitude modulation index (m_a) is the ratio of reference amplitude (A_m) to carrier amplitude (A_c).

$$m_a = A_m / (m-1) A_c$$

The frequency ratio (m_f) is ratio of carrier frequency (f_c) to reference frequency (f_m).

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$$m_f = f_c / f_m$$

IV. SIMULATION RESULTS AND DISCUSSION

A. Multi-Carrier Based SPWM MLI:

In phase disposition method all the carriers have the same frequency and amplitude. Moreover all the n-1 carriers are in phase with each other. It is based on a comparison of a sinusoidal reference waveform with vertically shifted carrier waveform as shown in Fig 4. This method uses n-1 carrier signals to generate n level inverter output voltage. All the carrier signals have the same amplitude, same frequency and are in phase. In this method three triangular carrier waves have compared with the one sinusoidal reference wave. A seven level cascaded H bridge multi level inverter is simulated in *MATLAB / SIMULINK* environment. The various method of the carrier based disposition analysis and gets the output waveform in a seven level inverter. SPWM generation circuit contains three carrier wave and one reference sine wave, then compared signal is given to the corresponds GTO to the multilevel inverter.

SPWM method is the extension of bi-level SPWM, one reference signal is used to compare to the carriers. 3 H-bridges being used for 7 level output voltage. This result has been obtained for the multi-cell converter in a seven-level configuration, which uses three series-connected cells in each phase. In 3-triangle method, therein, for 7-level inverter the A-phase duty cycle is compared with (3 in general) triangle waveforms.

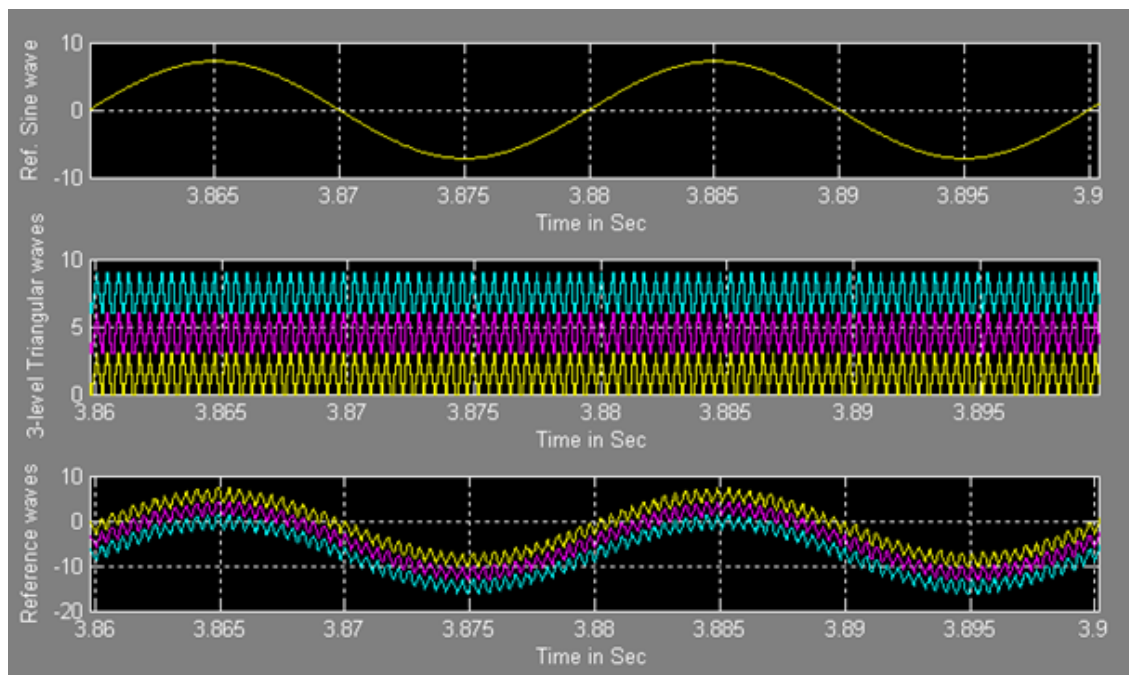


Fig. 4 Phase disposition modulation

Fig. 5 shows the FFT analysis for the Multi-Carrier Based SPWM MLI for the fundamental 50Hz. THD=0.35% and Fundamental being 203.6V.

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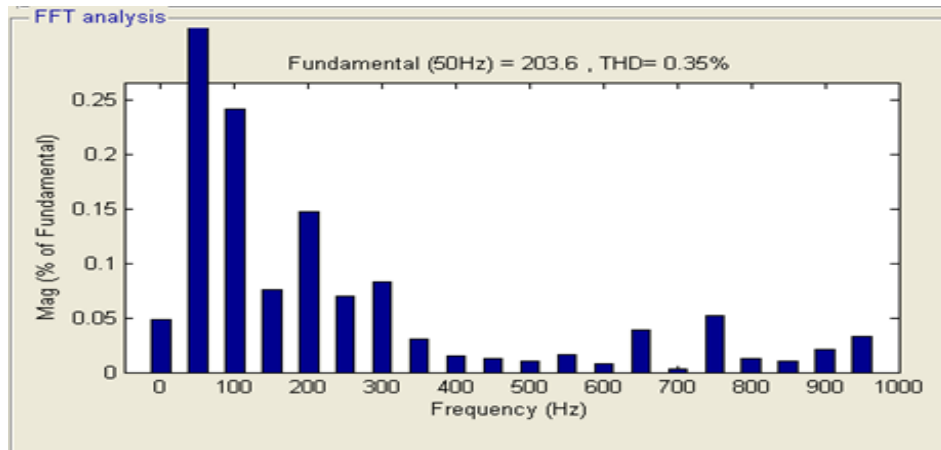


Fig.5 FFT analysis of Multi-carrier PWM output voltage

3-phase output voltage being connected to the Induction Motor Speed, Torque and Current characterizes being shown in Fig. 6.

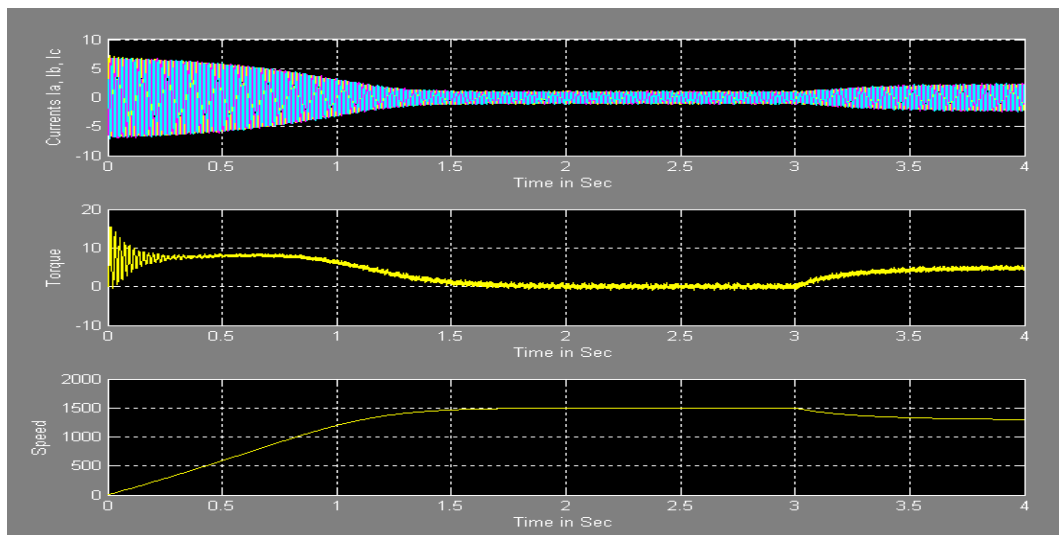


Fig.6 Multi-carrier PWM MLI fed IM Current, Torque and Speed Characteristics

B. Hybrid-Cascaded MLI connected to IM:

The modelled HCMLI and the firing angle results obtained from the resultant theory being used for obtaining 7-Level output voltage, Fig.7 is the SIMULIK model.

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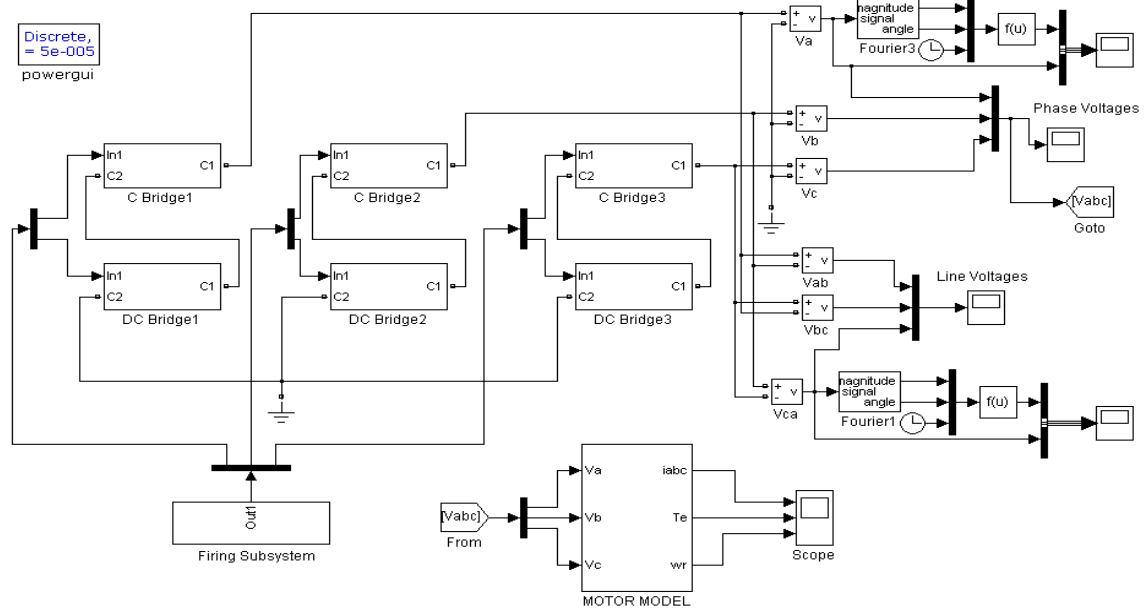


Fig.7 SIMULINK Model for the 3-Phase Hybrid Cascaded Multilevel Inverter

Fig. 8 shows the FFT analysis having THD = 23.61 and Fundamental component 203.5V.

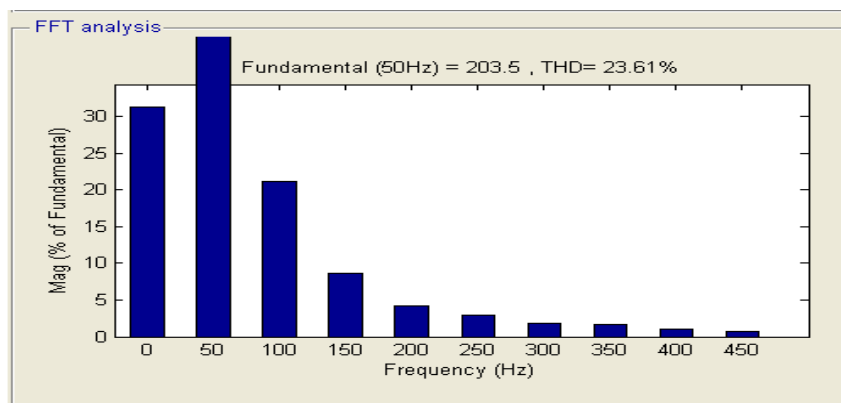


Fig.8 FFT analysis of HCMLI output voltage

Same Induction Motor is being connected for characteristic analysis and Fig. 9 show the Speed, Torque and Current characteristics.

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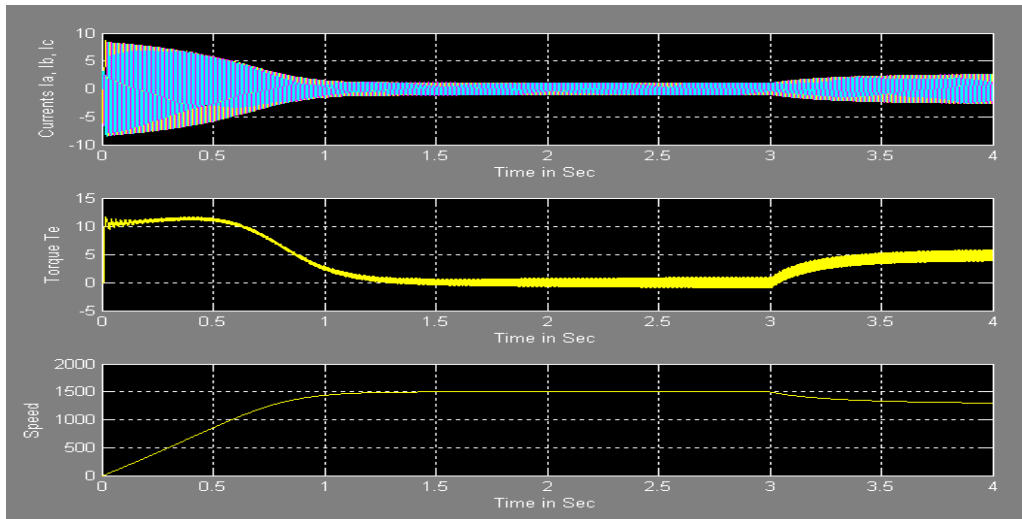


Fig.9 IM Stator Currents, Torque and Speed Characteristics

Analysis made from FFT is tabulated below for fundamental frequency of 50Hz

Table I
CONTROLLER FOR CAPACITOR VOLTAGE LEVEL

	Multi-carrier SPWM MLI	HCMLI
Fundamental Component	203.6	203
THD (in %)	0.35	23.61

For modulation frequency 2500Hz results are obtained, compared to the HCMLI configuration Multi-carrier SPWM MLI has low THD but is operating at higher frequency which is resulting thermal stresses on device. As the switching frequency of modulating wave increases THD is reduced but thermal stresses increases. HCMLI is comparably operating at low that is at 50Hz is resulting nearly sinusoidal and had THD of 23%.

For the same IM and load characteristics with no filter circuits employed in the output stage of both inverter circuits HCMLI has 12% more currents in starting currents but has less current ripple than Multi-carrier based SPWM. Speed characterises are similar in both inverters. Torque and current ripple can be reduced using filter circuits. Since HCMLI working at low switching-frequency results high output efficiency and low thermal stresses in switching devices.

V. CONCLUSION

This paper utilizing a method called hybrid cascaded H-bridge multilevel Inverter (HCMLI) by implemented using a single dc power source and capacitors. HCMLI using one power source for each phase while producing desired 7-level multilevel voltage waveforms is performed. A fundamental frequency switching control algorithm is being used. This paper showing the difference and comparison between modeling and simulation of a Multi-carrier based SPWM Multilevel Inverter and Low Switching Frequency Hybrid Cascaded Multilevel Inverter fed to an Induction Motor and analysis of Induction Motor currents, torque and speed characteristics.

REFERENCES

- [1] L. M. Tolbert, F. Z. Peng, and T. G. Habetler, "Multilevel converters for large electric drives", IEEE Trans. Ind. Appl., Vol. 35, no. 1, pp. 36–44, Jan./Feb. 1999.
- [2] J. S. Lai and F. Z. Peng, "Multilevel converters—A new breed of power converters", IEEE Trans. Ind. Appl., Vol.32, no.3, pp.509–517, May/Jun. 1996.
- [3] J.Rodriguez, J.Lai,andF.Peng, " Multilevel inverters: A survey of topologies, controls and applications", IEEE Trans. Ind. Electron., Vol.49,no.4, pp.724–738,Aug. 2002.



International Journal of Advanced Research in Electrical, Electronics and Instrumentation Engineering

(An ISO 3297: 2007 Certified Organization)

Vol. 2, Issue 12, September 2013

- [4] J. Rodriguez, S. Bernet, B. Wu, J. O. Pontt, and S. Kouro, “Multi-level voltage-source-converter topologies for industrial medium-voltage drives”, IEEE Trans. Ind. Electron., Vol. 54, no. 6, pp. 2930–2945, Dec. 2007.
- [5] P. Hammond, “A new approach to enhance power quality for medium voltage ac drives”, IEEE Trans. Ind. Appl., Vol. 33, no. 1, pp. 202–208, Jan./Feb. 1997.
- [6] W.A.HillandC. D.Harbourt, “Performance of medium voltage multilevel inverters”, Proc. IEEE Ind. Appl. Soc. Annu. Meeting, Phoenix, AZ, pp. 1186–1192, Oct. 1999.
- [7] Z.Du, L.M.Tolbert, J.N.Chiasson, B. Ozpineci, H.Li, and A.Q.Huang, “Hybrid cascaded H-bridges multilevel motor drive control for electric vehicles”, Proc. IEEE Power Electron. Spec. Conf., Jeju, Korea, pp. 1–6, Jun.18–22 2006.
- [8] Z. Du, L. M. Tolbert, and J. N. Chiasson, “A cascade multilevel inverter using a single fuel cell DC source”, Proc. IEEE Appl. Power Electron. Conf., Dallas, TX, Vol.1, pp.419–423, Mar. 19–23 2006.
- [9] Zhong Du, Leon M. Tolbert, Burak Ozpineci, John N. Chiasson, “Fundamental Frequency Switching Strategies of a Seven-Level Hybrid Cascaded H-Bridge Multilevel Inverter”, IEEE Trans. on Power Electronics, Vol. 24, no. 1, January 2009.
- [10] K.A.Corzine ,F.A.Hardrick, and Y.L.Familiant, “A cascaded multi-level H-bridge inverter utilizing capacitor voltages sources”, Proc. IASTED Int. Conf. Power Energy Syst., Palm Springs, CA, pp.290–295, Feb. 24–26 2003.
- [11] J. N. Chiasson, L. M. Tolbert, K. J. McKenzie, and Z. Du, “Control of a multilevel converter using resultant theory”, IEEE Trans. Control Syst. Technol., Vol. 11,no. 3,pp. 345–354, May 2003.
- [12] J.N.Chiasson, L.M.Tolbert, K.J.Mc Kenzie, and Z.Du , “ A new approach to solving the harmonic elimination equations for a multilevel converter”, Proc. IEEE Ind. Appl. Soc. Annu. Meeting, Salt Lake City, UT, pp. 640–645, Oct.12–16 2003.