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# Biodiesel Extraction and Evaluation of Emission Parameters of a DI Diesel Engine Fueled by Pure / Used Biodiesel with Diesel and Oil with diesel Blends at High Idling operations

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**ABSTRACT:** Biodiesel from pure and used oil is produced by transesterification process in this study. Quality of biodiesel is examined standards testing methods. Important fuel properties of biodiesel, such as heating value, cetane index, viscosity, and others are also investigated. A direct injection (DI) diesel engine is tested with biodiesel–diesel and oil–diesel blends for performance and emissions at high idling operations. Three fuel series are examined: pure biodiesel, used biodiesel and pure oil series. In all the series, fuels are blended with diesel 5–20 volume percentage. Engine performance is examined by measuring brake specific fuel consumption and fuel conversion efficiency. The emission of carbon monoxide (CO), hydrocarbon (HC), oxides of Nitrogen (NO<sub>x</sub>) and others are measured. Pure and used biodiesel blends show very similar fuel properties, engine performance and emissions. CO and HC emissions from biodiesel–diesel blends are significantly less than neat diesel fuel. Even pure oil up to 5% in diesel fuel can show significantly less CO emissions than that of diesel fuel. Up to 5% biodiesel and oil in diesel fuel, NO<sub>x</sub> emissions either can reduce or maintain similar level to that of diesel fuel.

## I. INTRODUCTION

Climate change and mitigation of greenhouse gas (GHG) emissions are of the primary motivations for biofuels research. Furthermore, the growing concern on environmental pollution caused by the extensive use of conventional nonrenewable fuels has led to search for more environment friendly and renewable fuels. Biofuels such as alcohols and biodiesel have been proposed as alternatives for internal combustion engines [1,2]. In particular, biodiesel has received wide attention as a replacement for diesel fuel because it emits less GHG and other pollutants. Biodiesel can reduce net carbon-dioxide emissions by 78% on a lifecycle basis when compared to conventional diesel fuel [3]. United States Environmental Protection Agency (US EPA) has done a comprehensive analysis of biodiesel impacts on exhaust emissions [4] mentioning that pure biodiesel can reduce HC as high as 70% and particulate matters (PMs) and CO about 50% when compared with conventional diesel fuel. A rapid expansion in production capacity is being observed not only in developed countries such as Germany, Italy, France, and the United States but also in developing countries such as Brazil, Argentina, Indonesia, and India. Interest in and expansion of the production of the renewable fuel have been fostered by mandates and financial incentives offered by governments. This interest can be mostly attributed to the commonly cited advantages of biofuels, especially that they can reduce the emission of gases responsible for global warming, promote rural development, contribute toward the goal of energy security, are renewable, and reduce pollution. Another feature that proponents of biodiesel put forward is that the fuel can be used without modification in engines currently in use. Several countries including Canada have already begun substituting the conventional diesel by



a certain amount of biodiesel. The use of biodiesel is being promoted by European Union (EU) countries to partly replace diesel fuel in order to reduce greenhouse effect and dependency oil. Meeting the targets established by the European Parliament for 2020 would lead to a biofuel market share of 10% [5]. Few Researchers has announced a new biofuel strategy (2% biodiesel in diesel for ground transportation and heating by 2012 and 5% by 2015). Biodiesel is mainly produced from different types of vegetable oils (e.g., rapeseed, soybean, canola, sunflower, palm oil, etc.). Canola/used canola oil is one of the leading feedstock for biodiesel production. Transesterification is regarded as one of the most efficient methods to produce biodiesel from vegetable oils due to its low cost and simplicity [6,7]. Thus, this study will choose canola oil as feedstock and use transesterification process to produce biodiesel. Many investigations have indicated that the use of biodiesel can result in a substantial reduction in PM, HC and CO emissions [8–11]. However, a slight increase in NO<sub>x</sub> emission is observed by most researchers when biodiesel is used [12–14]. Most of the researchers have found that the use of biodiesel instead of diesel can cause reduction in PM emissions [8–11,15,16]. Wu et al. [15] investigated the emission performance for five pure biodiesels on a Cummins ISBe6 DI engine with turbocharger and intercooler, and found that the related biodiesels could reduce PM emission by 53–69% on average compared with the diesel fuel. Lin et al. [16] also observed that there was significant reduction (ranging from 50% to 72.73%) in the smoke emission for eight kinds of biodiesels compared with petroleum diesel. A small portion of authors found that there was no difference in PM emissions for biodiesel relative to diesel [17,18], or even there was a bit increase [19,20]. According to most of literatures, it was a common trend that CO emissions could be reduced when diesel was replaced by pure biodiesel [8–11,21–23]. Krahl et al. [21] obtained about 50% reduction in CO emissions for biodiesel from rapeseed oil compared to low and ultra-low sulfur diesel. A higher reduction in CO emissions was reported by Raheman and Phadatare (up to 73–94% for the karanja biodiesel and its blends compared to diesel) [22], and by Ozsezen (86.89% for waste palm oil biodiesel and 72.68% for canola biodiesel) [23]. However, some literature showed the less reduction. For example, Utluand Kocak [24] obtained the reduction of around 17.13% than diesel fuel. Some authors found different trend at different load conditions; for example, An et al. [25] reported that although CO reduced at high load operations, it increased significantly at light load operations with the increase of biodiesel blend ratio. Surprisingly some authors reported the increase in CO emissions for pure biodiesel [26,27]. Banapurmatha et al. [26] observed higher CO emissions for jatropha, honge and sesame biodiesel compared to diesel on a single-cylinder, 4-stroke, DI diesel engine at a rated speed of 1500 rpm at 80% load. Macor et al. [27] reported a slight CO increase with biodiesel than diesel. Most literatures found reductions in HC emissions when pure biodiesel was fueled instead of diesel [11,15,16,26,28]. Wu et al. [15] reported that the five different biodiesels could reduce HC emission by 45–67% on average compared with diesel fuel. Puhan et al. [28] found that the average reduction in HC emissions was around 63% for biodiesel compared with diesel. But some authors reported the lower decreases, for example, in the range of 22.47–33.15% for the eight kinds of biodiesels from Lin et al. [16]. Ng et al. [11] showed that engine-out HC concentration reduced with increasing biodiesel content in blend and HC concentration of neat palm biodiesel was 26.2% lower than that of fossil diesel. However, Banapurmatha et al. [26] and Macor et al. [27] found higher HC emissions with different biodiesels compared to diesel fuel. In NO<sub>x</sub> emissions from biodiesel operation, there is a divided opinion or results in literatures. Many literatures believe that the use of pure biodiesel causes the increase in NO<sub>x</sub> emissions [12–14,16,23,29]. For example, a maximum of 15% increase in NO<sub>x</sub> emissions for neat biodiesel was observed at high load conditions as the results of 12% oxygen content of biodiesel and higher gas temperature in combustion chamber [29]. Ozsezen et al. [23] found that NO<sub>x</sub> could increase by 22.13% and 6.48%, respectively, by waste palm and canola biodiesels. Lin et al. [16] compared eight kinds of biodiesel mentioned above and found that using biodiesel in the diesel engine could yield higher NO<sub>x</sub> emissions, ranging from an increase of 5.58–25.97% when compared to diesel. Many others [26,28,30] reported that NO<sub>x</sub> emissions reduced when using biodiesel.

## II. MATERIALS AND METHODS

To produce biodiesel, pure canola oil and used/cooked canola oil are used as feedstock. Pure canola oil was purchased from a local supermarket and used canola oil was collected from research laboratory. Two main ingredients for biodiesel production were methanol and sodium hydroxide that were purchased. The physical and chemical properties of methanol and sodium hydroxide are shown in Table 1. A DI diesel engine was tested to examine its performance and emissions with biodiesel–diesel and canola oil–diesel blends at different volume proportions. The tested blends were B0 (diesel), B5 (5% canola biodiesel in diesel), B10 (10% canola biodiesel in diesel), B15 (15% canola biodiesel in diesel), B20 (20% canola biodiesel in diesel), UCB5 (5% used canola biodiesel in diesel), UCB10 (10% used canola biodiesel in diesel), UCB15 (15% used canola biodiesel in diesel), UCB20 (20% used canola biodiesel in diesel), C5 (5% canola oil in diesel), C10 (10% canola oil in diesel), C15 (15% canola oil in diesel) and C20 (20% canola oil in diesel).



Table. 1 The physical and chemical properties of methanol and sodium hydroxide

Chemical formula	CH <sub>3</sub> OH	NaOH
Molecular weight	32.04	39.997
Purity (%)	100	99
Flash point (°C)	12	–
Boiling point (°C)	64.5	1390
Autoignition temperature (°C)	464	–
Specific gravity	0.8	2.13
Vapor pressure (mmHg)	97 @ 20 °C	1 @ 739 (°C)
Melting point (°C)	–	318
pH (of a 5% solution)	–	14

### Biodiesel production and properties

The most commonly used method of biodiesel production is the transesterification of triglycerides with methanol in the presence of a catalyst, which gives biodiesel and glycerol (by-product). The basic biodiesel reaction and flow chart of biodiesel production is illustrated in Fig. 1. The procedure to make biodiesel followed in this study is similar to that described in [45]. The final collection efficiency is 86% for pure canola oil and 90%

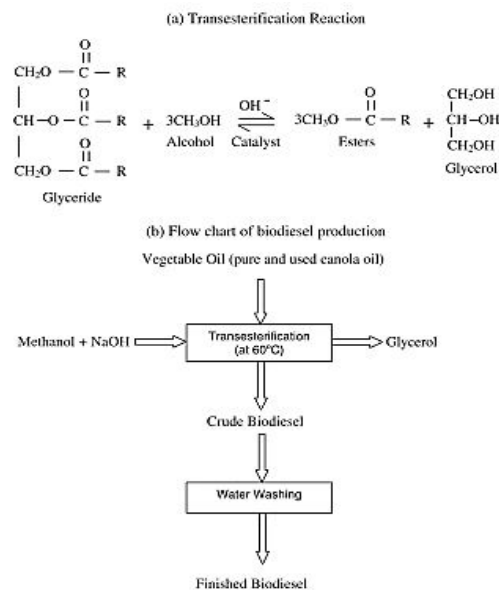


Fig. 1. Basic biodiesel reaction: (a) transesterification reaction and (b) flow chart of biodiesel production.

The basic biodiesel reaction and flow chart of biodiesel production

### Engine test

Fig. 2 shows the schematic diagram of engine experiment. The engine used in this study was a four-stroke two-cylinder naturally aspirated DI diesel engine. All experimental data were taken after engine warm-up (about 20 min after start). In this condition, there was almost no fluctuation of emissions. Tests were carried out at the warmed up condition of the engine under high idling (i.e., 1200 rpm) and with 15% engine loads, as summarized in Table 2. Loads were measured by a water brake dynamometer. Fuel temperatures are important, which affect viscosity and atomization of canola oil and other biodiesels. Fuel temperatures are kept constant keeping the engine room temperature constant at 20 °C for all the tests. The fuel supply system was modified to switch between the diesel fuel used as a standard and the test fuels. The engine was started using diesel; once the engine warmed up, it was switched to biodiesel–diesel or canola oil–



diesel blends. After concluding the tests the engine was again switched back to diesel before stopping the engine until the blends were purged from the fuel line, injection pump and injector. Engine load and fuel consumption were measured to calculate brake specific fuel consumption (BSFC) and fuel conversion efficiency (GF) of the engine. The difference in engine torque as well as power at a certain engine speed for different fuels was insignificant; that is why only one value of engine power at each speed for biodiesel– diesel and canola oil–diesel blends.

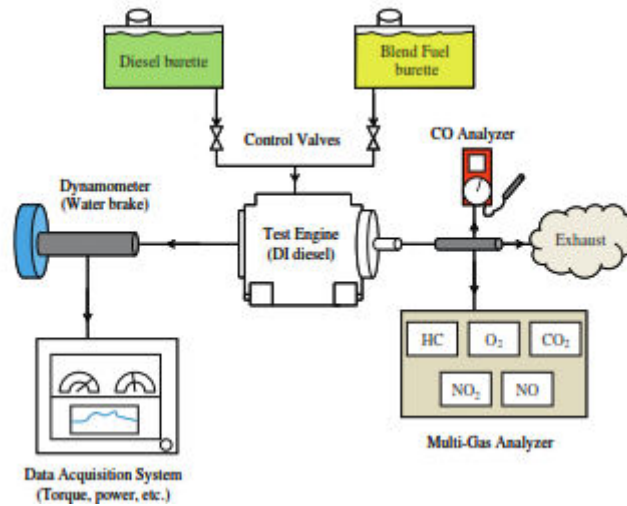


Fig. 2 shows the schematic diagram of engine experiment.

Table 2 Fuel properties of biodiesel–diesel and canola oil–diesel blends.

Fuel	Density (kg/m <sup>3</sup> )	Viscosity (cSt)	Heating value (kJ/kg)	Cloud point (°C)
B0	844	2.68	44,861	-26
B2	845	2.72	44,711	-23
B5	846	2.89	44,601	-22
B10	848	3.07	44,297	-22
B20	850	3.22	43,715	-19
B100	870	4.26	39,369	-3
UCB	845	2.72	44,732	-22
2	846	2.77	44,556	-22
UCB	849	2.93	44,266	-22
5	851	3.07	43,643	-20
UCB	872	4.22	39,289	-4
10	846	2.8	44,826	-26
UCB	848	2.98	44,653	-26
20	852	3.63	44,398	-26
UCB	858	4.28	43,758	-26
100				
C2				
C5				
C10				
C20				

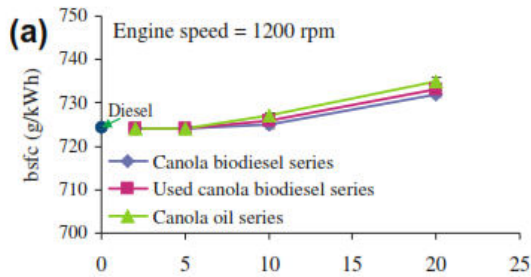


Fig. 4 The variation of BSFC of the engine

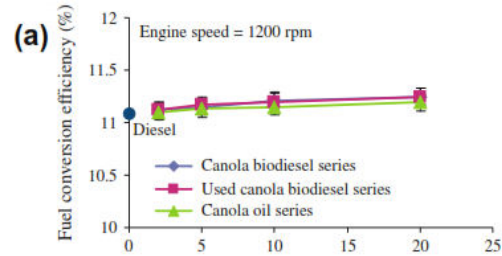


Fig. 5 Fuel Conservation Efficiency

### III. RESULTS AND DISCUSSION

#### Engine performance

Fig. 4 shows the variation of BSFC of the engine with canola biodiesel–diesel, used canola biodiesel–diesel and canola oil–diesel series at engine speed of 1200 rpm, At this speed, there is no significant increase in BSFC with biodiesel–diesel and canola oil–diesel series up to 15% blends; however, 20% blends of biodiesel and canola oil with diesel show about 1.1–2.3% BSFC increase, respectively, than neat diesel operation at different engine speeds. B20 and UCB20 have, respectively, 2.55% and 2.7% lower heating value than diesel fuel. This indicates that biodiesel–diesel blends have higher fuel conversion efficiency than that of diesel fuel. The variation of fuel conversion efficiency of the engine with various fuels is demonstrated in Fig. 5. Canola oil–diesel series has pretty similar efficiency to that with diesel at each engine speed. There is no significant change in fuel conversion efficiency with biodiesel–diesel series up to 5% blends in comparison to diesel at all engine speeds. However, 10% and 20% biodiesel blends show 1–1.5% efficiency increase than neat diesel operation. A little higher efficiency with biodiesel–diesel series at each engine speed induces less BSFC increase of these blends than they should have been according to their calorific values. Furthermore, the higher efficiency with biodiesel–diesel series than diesel indicates that blend fuels combustion is better than diesel fuel combustion. This is attributed to oxygen content of biodiesel. Due to better combustion with biodiesel, less emission of CO and HC is expected.

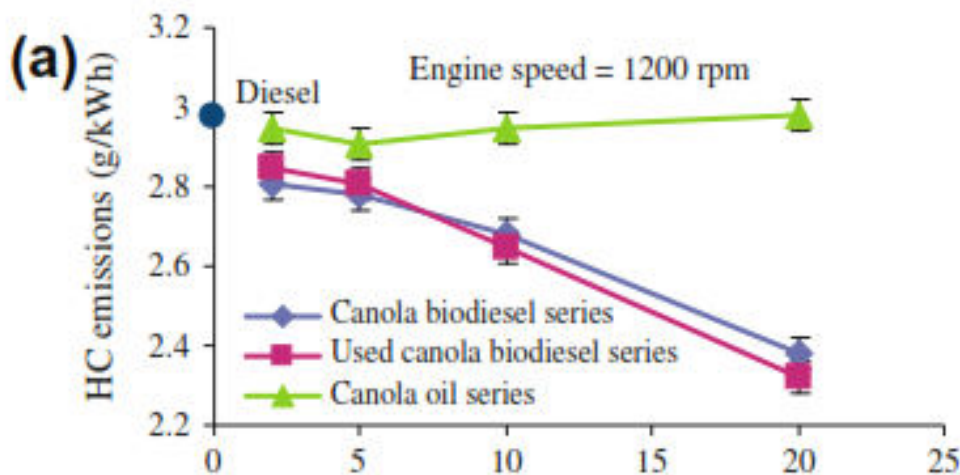


Fig. 6 shows CO emissions

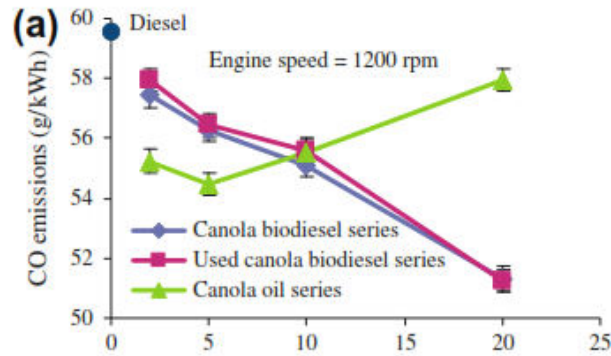


Fig. 7 HC emissions

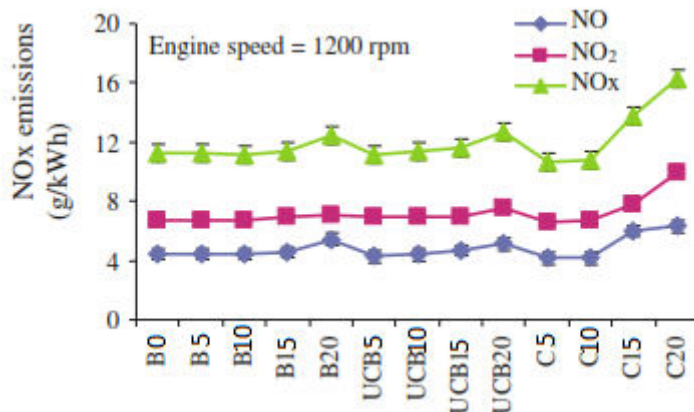


Fig. 8NOx emissions

**Emissions**

The emissions of CO, HC, and NOx are illustrated in Figs. 6–8. Fig. 6 shows CO emissions at the engine speed of 1200 rpm for various fuels. At 1200 rpm, diesel fuel produces the maximum CO (59.53 g/kW h), which decreases gradually with biodiesel–diesel blends and becomes the lowest (51.24 g/kW h) for B20 orUCB20 (approximately 14% lower). However, CO emissions with canola oil–diesel series are different than the biodiesel–diesel series. There is a gradual decrease in CO emissions up to C5, which is even better than the biodiesel–diesel series. The main observations from CO emission results are as follows:

- (1) the higher the engine speed, the lower the CO emissions for all of the fuels. This is due to better mixing of air and fuels at higher speeds for higher turbulence;
- (2) the higher the biodiesel percentage in biodiesel–diesel blends, the lower the CO emissions. This could be due to higher O<sub>2</sub> concentration in the air–fuel mixture, which can improve combustion and enhance further CO oxidation;
- (3) canola oil–diesel blends show lower CO emissions than diesel;
- and (4) the higher the engine speed and the lower the canola oil percentage in diesel fuel perform better than similar biodiesel–diesel blends, such as up to C5 at 1200rpm. The lower percentage of canola oil in the blends has very similar fuel properties to diesel, however a bit of O<sub>2</sub> can help better combustion and lower CO emissions than diesel. On the other hand, the question is why this is better than similar biodiesel–diesel blends, when biodiesel has similar O<sub>2</sub> content in it.



Higher heating value of C5 than B2, UCB2 or B5, UCB5 (Table 2) may be one of the main reasons. The degradation of performance in CO emissions with canola oil–diesel blends with respect to biodiesel–diesel blends could be attributed to improper combustion due to shorter combustion period at higher engine speeds. Lower cetane number of canola oil–diesel blends will increase ignition delay that causes higher amount of fuel accumulation before combustion starts. Higher viscosity of canola oil–diesel blends will degrade spray characteristics especially for low injection pressure engines (e.g., the one used in this work), and cause improper mixture formation. Higher amount of improper mixtures and shorter combustion period make canola oil–diesel blends combustion poorer. It seems that proper mixture formation at higher engine speeds plays an important role for better combustion and lower CO emissions. Higher biodiesel–diesel blends can supersede similar canola oil–diesel blends at higher engine speeds in proper mixture formation and combustion. Fig. 7 demonstrates HC emissions at specific speed for various fuels. At 1200 rpm, diesel fuel produces 2.98 g/kW h of HC; it decreases gradually with biodiesel–diesel blends and becomes 22% lower for UCB20 and 20% lower for B20. No significant change is observed for canola oil–diesel series. At this speed, canola oil–diesel series shows approximately 6% increase than that of diesel. Here also:

- (1) the higher the engine speed, the lower the HC emissions for all fuels. This phenomenon can be attributed to better mixing of air and fuel at higher engine speeds;
- (2) the higher the biodiesel percentage in biodiesel–diesel blends, the lower the HC emissions. This is due to the fact that the higher O<sub>2</sub> concentration in the air–fuel mixture can help enhance oxidation of unburned hydrocarbons;
- (3) canola oil blends are not a good candidate for HC reductions; although at lower speeds, there is no significant change in HC emissions, at the engine speed of 1200 rpm, HC is increased by 6% than diesel and a lot more than biodiesel–diesel series. It seems that detrimental cetane and viscous effect have overturned the positive effect of O<sub>2</sub> content in canola oil–diesel blends at higher engine speeds again due to shorter combustion period, which is in agreement with CO emissions. Fig. 8 illustrates NO, NO<sub>2</sub> and NO<sub>x</sub> emissions at 1200 rpm speed for various fuels. At light load operations, the engine runs at a very lean state and with a small biodiesel or canola oil blends. Hence, higher amount of NO<sub>2</sub> is produced at light load operations. This suggests that a proper care is needed to report NO<sub>x</sub> emissions from biodiesel combustion, especially at high idling operation. This also suggests that NO<sub>x</sub> abatement technology must include a system to address both NO<sub>2</sub> and NO reduction.

#### IV. CONCLUSIONS

Pure and used canola biodiesels have been produced and their quality and fuel characteristics have been investigated. An experimental investigation has been conducted to explore the performance and emissions of biodiesel and canola oil blends at high idling operations on a small DI diesel engine. The results obtained suggest the following conclusions:

- (1) Quality biodiesels are produced from pure and used canola oil by base catalyst transesterification process that satisfies ASTM standard. The conversion rate is 100% and collection efficiency 86–90%. Its cetane index is about 50 and heating value about 10% less than diesel fuel.
- (2) The viscosity of pure canola oil is very high and it reduces to about 10 cSt level at 90 °C which is higher than ASTM limit of 6 cSt. However, up to 30 vol.% of canola oil in diesel shows the viscosity values less than ASTM limit. Its heating value is pretty similar to biodiesels.
- (3) There is no fuel penalty up to 5% blend of biodiesel or canola oil in diesel, but with 20% blends the fuel penalty is about 1.1–2.3% at different speeds. Biodiesel–diesel and canola oil–diesel blends show higher fuel conversion efficiency than that of neat diesel.
- (4) CO emissions for all fuels are lower at higher engine speeds, and the higher the biodiesel percentage in biodiesel–diesel blends, the lower the CO emissions are. B20 or UCB20 shows average CO reduction of 13%. Up to 5% of canola oil in the blends, CO emissions are even lower than similar biodiesel–diesel blends, but for higher canola oil in the blends, CO is higher than that of similar biodiesel–diesel blends but lower than diesel.
- (5) HC emissions for all fuels are also lower at higher engine speeds, and the higher the biodiesel percentage in biodiesel–diesel blends, the lower the HC emissions are, a similar trend to that of CO emissions. B20 or UCB20 shows average HC reductions of 22%. There is a small reduction in HC up to C5 at lower speeds, but higher blends of canola oil and higher speeds deteriorate HC emissions.
- (6) Up to 5% biodiesel and canola oil in the blends, there is no increase in NO, NO<sub>2</sub> and NO<sub>x</sub> emissions, in fact canola oil up to 5% in the blends shows a little reduction of NO, NO<sub>2</sub> and NO<sub>x</sub> emissions than diesel. However, B20 or UCB20 has 12–26% NO<sub>x</sub> increase and C20 shows 44–58% NO<sub>x</sub> increase at different engine speeds. NO<sub>2</sub> production at high idling operations is found very significant and even higher than NO production and its share in total NO<sub>x</sub> is more than 50%.



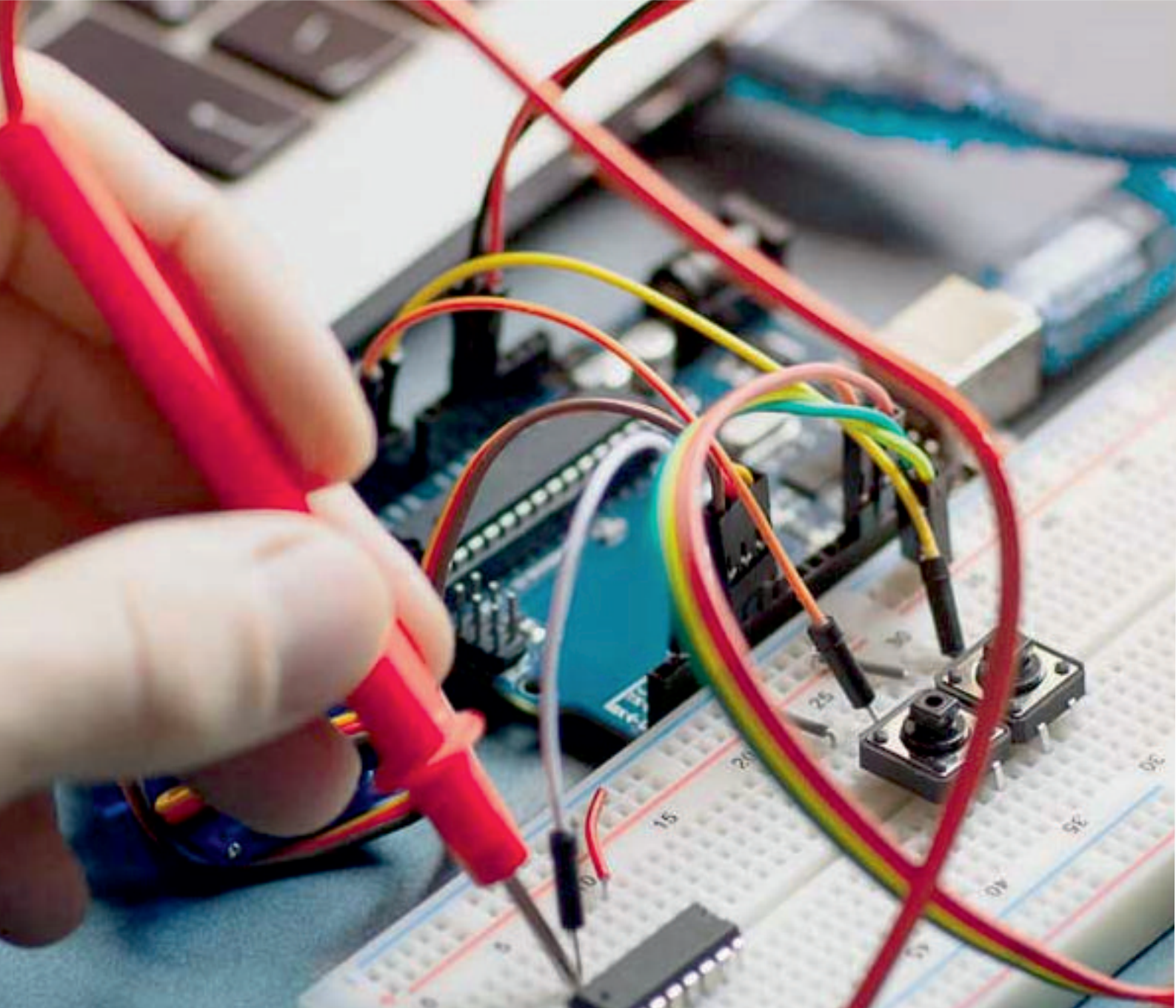


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