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# Single Switch Positive Output Boost Converter With Switched Inductor Cell

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**ABSTRACT:** A single switch positive output boost converter with switched inductor cell is introduced. In order to improve the gain a switched inductor concept is used. A non-isolated type positive output fifth-order dc-dc boost converter having a capacitor diode cell. This topology is developed from the existing fourth-order boost converter (FOBC) by appropriately inserting a charge pump cell. Analysis and controller design for positive output boost converter is done. The dc-dc converter exhibits continuous output-port current and it results in the reduction of peak to peak ripple current in the output capacitor. This topology is essentially derived from a fourth-order boost converter. Compared to fourth-order boost converter, the topology offers enhanced voltage gain with reduced switch voltage stress. The converter has an advantage of continuous output-port current over existing boost topologies, which reduces the output capacitor current stress. The simulation is done by using MATLAB/ SIMULINK software. The converter is controlled using PIC16F877A. The experimental results obtained from a converter prototype confirm the theoretical considerations and the simulation results.

**KEYWORDS:** switched inductor cell, charge pump cell.

## I. INTRODUCTION

Power electronics-based converters have been extensively used in many applications. For example, renewable energy generation systems, sources such as fuel cells and solar panels, and other dc-sources. Converters for fuel cell or solar power systems typically need a boost-type converter to convert a low-level dc voltage obtained from fuel cells or solar cells into a high-level dc voltage. Renewable energy has more attention on the recent years for increasing the cost of the fossil fuel. The energy sources are solar panel fuel cells and output voltage of these energy sources are low and variable.

A

number of high step-up converter topologies have been used to get the high voltage gain with suitable duty cycle. Nowadays the necessity of high-frequency dc-dc power conversion is gradually increasing in many applications such as automobile headlamps, X-ray systems, electric vehicles, photovoltaic systems, and uninterruptible power supplies, etc. Designers in the development of dc-dc converters for point-of-load applications with the following goals are higher voltage gain, higher power density, and better conversion efficiency. Conventional boost dc-dc converter is a well-established topology for the applications demanding higher load voltages. However, achieving higher voltage boosting at full-load imposes a constraint on the efficiency. Priyabrata Shaw [1] introduces Analysis and Controller Design for Positive Output Boost Converter with Low Current Stress on Output Capacitor non-isolated type positive output fifth-order dc-dc boost converter is proposed in this paper. This topology is developed from the existing fourth-order boost converter (FOBC) by appropriately inserting a charge-pump cell. Compared to FOBC, the proposed topology offers enhanced voltage gain with reduced switch voltage stress. P. Shaw [2] introduces Positive output boost converter with low current stress on output capacitor. A non-isolated type positive output fifth-order dc-dc boost converter is proposed. Compared with basic boost converter, the proposed topology is capable of offering higher voltage gain with lower voltage stress on switch. Anmol Ratna Saxena [3] introduces a design of robust digital stabilizing controller for fourth-order boost DC DC converter a quantitative feedback theory approach. In this paper, we have proposed a quantitative feedback theory based robust digital voltage mode controller for a fourth-order boost dc dc converter operating in continuous conduction mode. The fifth-order boost [4] topologies exhibiting gain find limited utility in point-of-load applications due to lack of common ground, inverted load voltage polarity, highly pulsating source current, and more switching devices, etc. This fifth-order boost converter which successfully overcomes the limitations. The basis for evolution of this topology is addition of a charge pump capacitor with a diode to the converter. A limitation in some of these circuits is that the load ground is isolated from the source ground. So, this



converter is not suitable in applications needing voltage gain of FOBC, but with common ground. P. Shaw [5] introduces analysis and design of CD-cell-based fifth-order boost converter with robust stability considerations illustrating fifth-order boost topologies exhibiting gain to find limited utility in point-of-load applications due to lack of common ground, inverted load voltage polarity, highly pulsating source current, and more switching devices, etc. The fifth-order boost converter which successfully overcomes the enlisted limitations. Several voltage lift techniques [6] has used to improve the gain and efficiency like interleaved concepts. The voltage lift techniques used to convert the converter into high power application by lifting the voltage. Omar Abdel-Rahim [7] introduces a boost converter with high dc gain as a solution for partial shading of photovoltaic (PV) module. Switched inductor boost converter (SIBC) is introduced by replacing the inductor of the boost converter with a switched inductor branch. As a result, the conversion gain ratio can be increased. The proposed converter is used as an interface between the PV system and the load. A Maximum Power Point Tracking (MPPT) control is applied to extract the maximum power of the PV module. This paper introduces switched inductor boost type with PV module. With reference to the above-mentioned papers to overcome the drawbacks a Positive output boost converter with low current stress on output capacitor is introduced. Analysis and design of positive output boost converter [1] is taken as the base paper. In order to improve the efficiency and gain a switched inductor concept is implemented compared with the basic converter.

**II.METHODOLOGY**

In the fig. 1 shows the single switch positive output boost converter with switched inductor cell operated in two modes. The positive output boost converter has only a single switch. The switch operated in frequency of 50kHz. The output voltage is higher than the input voltage. The boost converter boosts their input voltage.

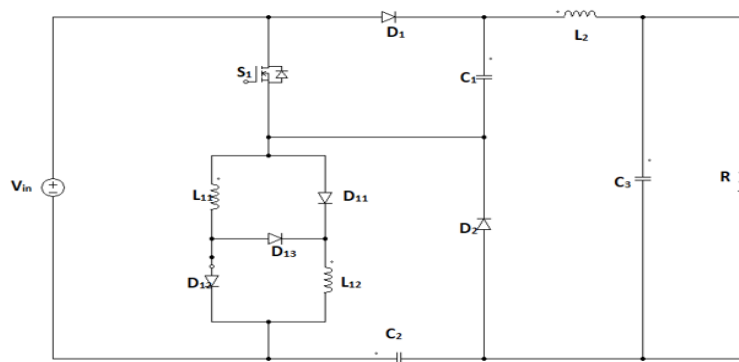


Fig. 1 Switched inductor based positive output boost converter

**III.MODES OF OPERATION**

In the fig. 2 shows the mode 1 operation. In this mode, switch S1 is turned on. The diode D1, D2 and D3 are in reverse biased and all other diodes are forward biased. The input voltage source charges three inductors L1, L2 and L3 and are utilized to drive the load-R. The capacitor C2 feeds the load and supplies current to the loads and also C1 discharges. Meanwhile C2 being discharged to load.

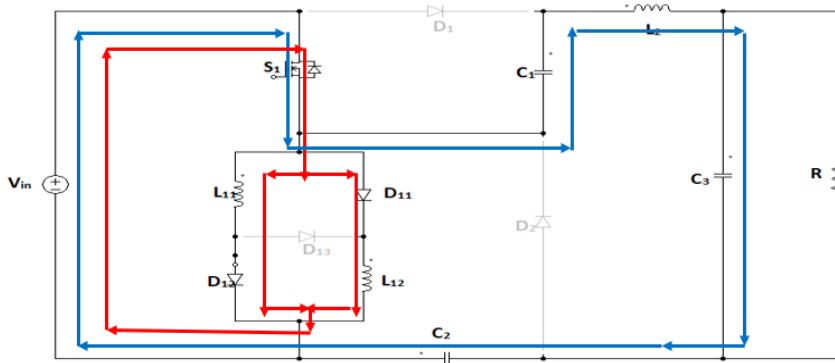


Fig. 2 Operating circuit of mode 1

In the fig.3 shows the mode 2 operation. In this mode  $S_1$  is in off condition. The diode  $D_1$ ,  $D_2$  and  $D_{13}$  are simultaneously forward biased condition and all other diodes are reverse biased. The stored energy in the inductors  $L_{11}$ ,  $L_{12}$  and  $L_2$  are discharged and are utilized to drive the load- $R$  and charge the intermediate capacitors  $C_1$  and  $C_2$ .

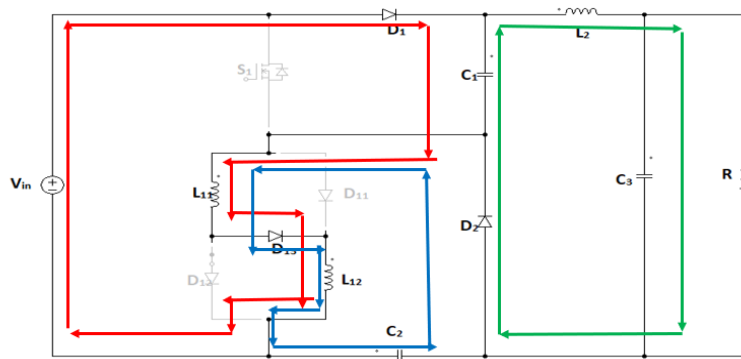


Fig. 3 Operating circuit of mode 2

In the fig. 4 shows the theoretical waveforms of a single switch positive output boost converter with switched inductor cell.

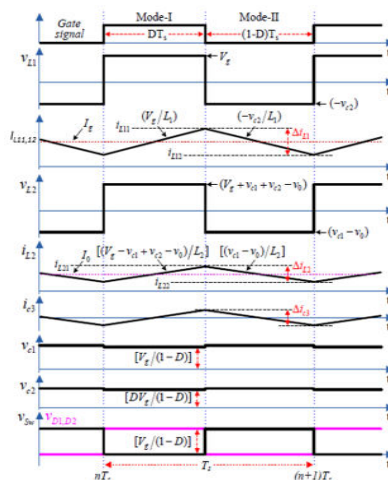


Fig. 4 Theoretical wave form of POBC



**IV.DESIGN OF COMPONENTS**

In order to operate the converter, its components should be designed properly. It consists of inductors and capacitors. The design of positive output boost converter with input voltage is taken as 36V. The switching pulses are at the rate of 50kHz and the duty ratio of 47% is fixed. The output voltage of the converter is  $V_0$  is equal to 142V with a output power of 200W. The output current of the converter is  $I_0$  is 0.42A.  $D$  is the duty ratio of the switch which is fixed. The current ripple is taken as less than 40% of inductor current. Resistance is  $100\Omega$ .

$$Gain = \frac{V_0}{V_{in}} = \frac{142}{36} = 3.78 \tag{1}$$

Consider the positive output boost converter with the duty cycle  $D$  which is equal to 0.47. The current ripple of inductor is taken as 40% of inductor current. Current through inductor  $L_{11}$  is

$$I_0 = \frac{V}{R} \tag{2}$$

$$I_{L11} = I_0 * \frac{1 + D}{1 - D} \tag{3}$$

$$L_{11} \geq \frac{V_{in} * D}{f * \Delta I_{L11}} \tag{4}$$

Current through inductor  $L_2$  is

$$I_{L2} = I_0 = \frac{V}{R} \tag{5}$$

$$L_2 \geq \frac{V_{in} * D}{f * \Delta I_{L2}} \tag{6}$$

The value of inductor is set as  $L_{11}$  and  $L_{12}=205\mu H$ . The value of inductor is set as  $L_2 = 1100\mu H$ . Consider the three capacitors  $C_1$  and  $C_2, C_3$  with same duty ratio. The capacitor values are given below. The voltage ripple of capacitor is taken as 1% of capacitor voltage. Voltage across the capacitor  $C_1$  is

$$V_{C1} = \frac{V_{in}}{1 - D} \tag{7}$$

$$C_1 \geq \frac{V_0 * D}{f * R * \Delta V_{C1}} \tag{8}$$

Voltage across the capacitor  $C_2$  is

$$V_{C2} = \frac{V_{in}}{1 - D} \tag{9}$$

$$C_2 \geq \frac{V_0 * D}{f * R * \Delta V_{C2}} \tag{10}$$

Voltage across the capacitor  $C_3$  is

$$V_{C3} = V_0 \tag{11}$$

$$C_3 \geq \frac{V_0 * D * (1 - D)}{8 * (1 + D) * f^2 * L_2 * \Delta V_{C3}} \tag{12}$$

The capacitor  $C_1$  and  $C_2$  taken as  $100\mu F$  and  $C_3$  is taken as  $220\mu F$ .

**V.SIMULATION RESULTS AND ANALYSIS**

Simulation parameters for a positive output boost converter is chosen based on the design of components. The switches are MOSFET with constant switching frequency of 50kHz. Simulation parameters of POBC are input voltage  $V_{in}$  is 36V, Rated power  $P_0$  is 200W Inductor  $L_{11}$ ,  $L_{12}$  is  $205\mu H$ , Inductor  $L_2$  is  $1100\mu H$  and Capacitor  $C_1$ ,  $C_2$   $100\mu F$ ,  $220\mu F$ . Fig. 5(a). shows the simulation result of input current and input voltage of the converter and  $I_{in}$  is 5.41A. The input current ripple of the converter is 0.02A.

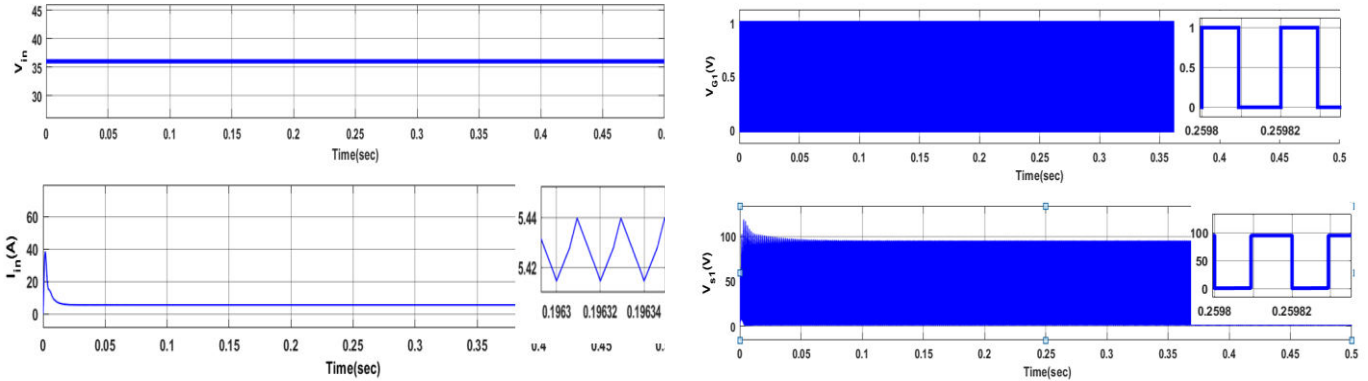


Fig. 5(a)Simulation time vs Input Voltage and Input Current(b)Simulation time vs Switching pulse and Voltage stress

Fig. 5 (b). shows gate pulse and voltage stress across the switchS1. The duty ratio of switch S1 is equal to 0.47. The switchingfrequency is chosen as 50kHz. Voltage stress across switch is95V. Fig. 7. shows the output voltage  $V_0$  and output current  $I_0$ .The output voltage is measured as 137V and it has outputvoltage ripple of 0.005V. The output current is measured as1.37A and current ripple of 40 $\mu$ A.

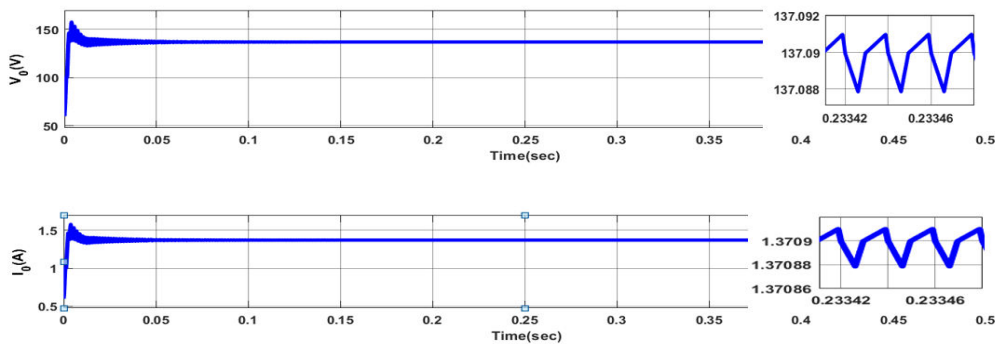


Fig. 7Output voltage and Output current

ANALYSIS:Analysis of positive output boost converter is carried out byconsidering parameters like efficiency, voltage gain.

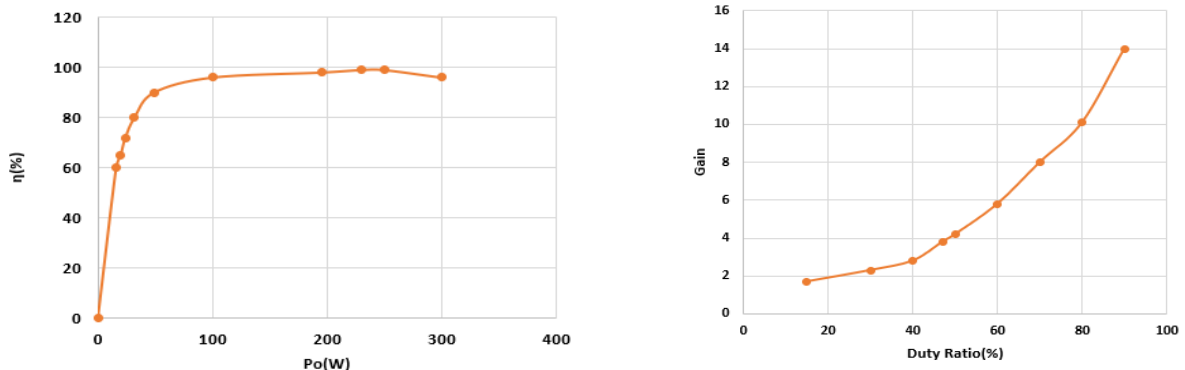


Fig .8(a)Efficiency Vs Output power with R load(b)Voltage Gain Vs Duty ratio

Efficiency of a power equipment is defined at any load asthe ratio of the power output to the power input.Fig. 8(a). Showsthe efficiency Vs output power with R load. Here the resistiveload is varied. switched inductor based positive output boostconverter has efficiency of 95%`Voltage Gain is defined at any load as the ratio of outputvoltage to input



voltage. Here the voltage gain increases for an increase in the duty ratio. Fig. 8(b). shows the analysis of duty ratio with gain. Here the duty ratio increases gain of the converter has also increased. The switched inductor based positive output boost converter has improved gain.

**VI. HARDWARE IMPLEMENTATION**

A prototype of POBC converter with input voltage of 5V is implemented. It consists of control circuit, driver circuit and power circuit. Control circuit is composed of PIC microcontroller and its power supply. The control pulses for MOSFET switches are generated using PIC microcontroller. The pulses from microcontroller are amplified by driver circuit which is composed of TLP250H. It also provides isolation between control and power circuit. The experimental setup of positive output boost converter is done through two stages. First the program is written in microC for generating gate pulses for switching devices. The program is verified and frequency is checked by simulating it in the Proteus software. The program is burned to the microcontroller (PIC16F877A) using the software micro programming suit for PIC. The switches used are MOSFET IRF640 along with its driver TLP250H. In power circuit an input of 5V is given to the converter. The switches used are IRF640. The pulses obtained from the microcontroller is fed to the interfacing circuit and the amplified pulse is given to the gate terminal of the MOSFET. The diodes used are 10A10NSL. The output voltage obtained is given to the digital storage oscilloscope (DSO). Fig. 9(a). shows the interfacing with controller circuit and experimental setup for the converter circuit. The controller circuit consists of PIC16F877A micro controller and crystal oscillator. It is used to select clock frequency for controller. A 5V supply is given to the controller and output of controller is given to interfacing circuit. The experimental setup for converter circuit is shown in fig. 9. It consists of power circuit and driver circuit. The output of the converter is shown in the digital storage oscilloscope. Fig. 9(b). shows the experimental result of the converter. The prototype is designed for 5V input with output of 19V. Here the output is obtained as 18.8V

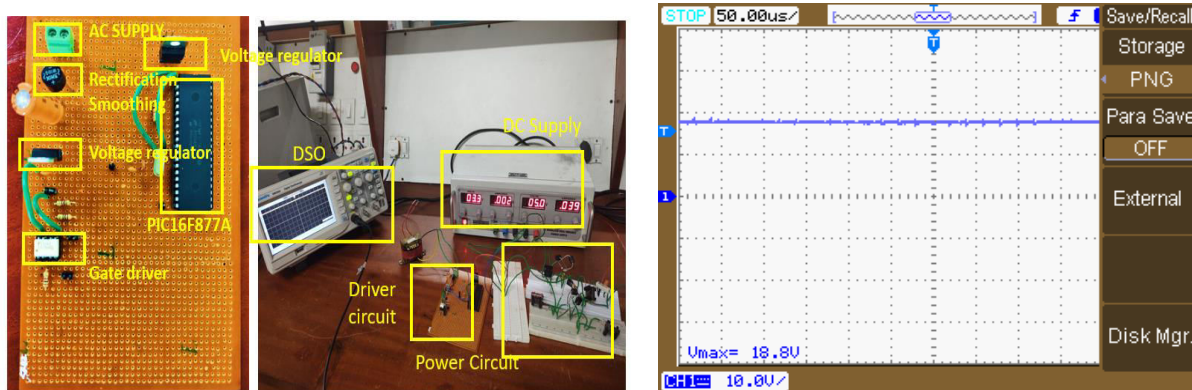


Fig. 9(a) Hardware implementation (b) Output voltage

**VII. CONCLUSION**

A single switch positive output boost converters with switched inductor cell are widely used for the renewable energy applications. The charge pump cell concept is used to improve the gain of the converter. It has low voltage ripple. The converter has low output capacitor current stress. The efficiency of the converter is low comparatively. It has a continuous input current. The voltage stress across the switch one is low. From the simulation results the voltage gain of the proposed converter is increased to 3.78 and efficiency of 95% for this converter for an input of 36V. The converter offers low voltage ripple of 0.005V. The design and simulation are done. Design and operation is flexible. The control of the proposed converter is implemented using PIC16F877A microcontroller. Converter prototype of 3.6W provides the expected performance with an output voltage of nearly 19V, considering the drop across the components. The overall analysis confirms that the proposed converter can be used in applications such as photovoltaics, electric vehicles, solar panel fuel cell etc.

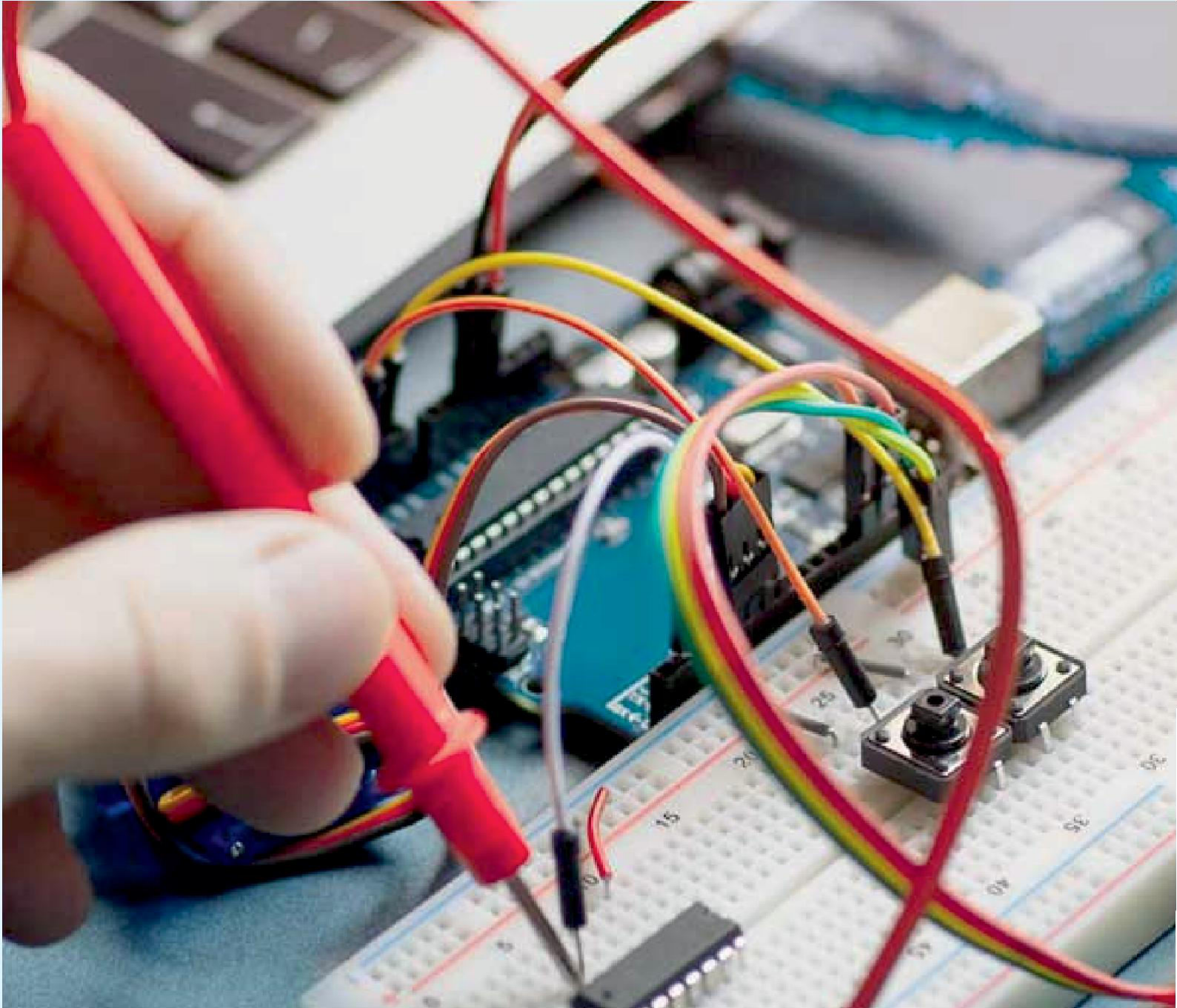
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