

(A High Impact Factor, Monthly, Peer Reviewed Journal)

Website: <u>www.ijareeie.com</u> Vol. 7, Issue 8, August 2018

SVPWM Based BLDC Close loop drive

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ABSTRACT: A brushless dc motor is categorized by high efficiency with good life time. Designed Bldc motor requires accurate speed and to recover rapidly from any turbulences for high performance, and sensitive to motor parameter variants. Many different speed controllers are widely used to run the motor for proper reference speed. In this present work, the current control technique are use to control the speed and position of BLDC motor. This method plays an important role, in the hardware implementation of position and speed control of BLDC motor. the error signals of currents achieved are fed to the rotor reference frame transformation (abc–dq) which develops the d-q currents. The position and speed of BLDC motor are control using d-q voltage which obtained from d-q current and fed to space vector PWM modulator.

KEYWORDS: PI current control, BLDC motor, Space vector PWM

I.INTRODUCTION

In recent years, smart control technology ,permanent magnet resources, computer technology, and power electronics technology, mostly the power switch component technology has been fast development, and it rested an important substance for the research and manufacture of the permanent magnet brushless DC motor (BLDCM). The BLDCM widely used in the servo mechanism , field of CNC machine tool, robots, because of its small size, control of high accuracy, easy maintenance. The modelling, simulation and analysis of a BDCM drive. The simulation included the real-time model ,state space model of the motor and speed controller of the inverter switches. Specific attention wasfunded to the motor large- and small-signal dynamics and motor torque pulsations. (1) In current control technique, the d-q current are drive using rotor reference frame transformation (abc–dq) error signals of currents obtained are fed to the which drive the d-q currents. The position and speed of BLDC motor are control using d-q voltage which obtained from d-q current and fed to space vector pwm modulator.[3] This paper realisedMatlabsimulink models Ofthe different control techniques like Sinusoidal Pulse Width Modulation (SPWM) and Space Vector Pulse Width Modulation (SVWM) delivered with proportional Integral (PI).[7]

A tuning methods of a PI speed controller for separatelyexcited Direct current motor is presented, based on Empirical Ziegler-Nichols tuning formula and improved Ziegler-Nichol PI tuning formula. Both these methods are compared on the basis of output response, minimum overshoot, and minimum settling time for speed demand application of BLDC motor.[10] as BLDC motor have a Trapezoidal BEMF so a many rotor referenceframe technique is not valid in this motor but in this paper we can apply the technique of abc -dq transformation in current control. when compared to other techniques this technique is advantages like Speed and position controller of BLDC motor at lower voltage ratings, high speed at low voltages, and accuracy in position control, reliability with high efficiency and also advantageous for most of the Hardware motor control.

II.PROPOSED MODEL

In this proposed model we can controlled the position and high speed can be achieved accurately at lowinput voltages. The rotor transformation technique cannot be applied because the back EMF of BLDC motor is trapezoidal. This paper, discusses the position and speed control of BLDC motor. without change in inductance in bldc motor we can use the rotor transformation technique. In proposed model the BLDC motor are use to Space Vector Pulse Width Modulator along with Current Controller in which rotor reference frame is downed for speed and position control. The machine is



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characterised by its equivalent circuit, which comprises of stator resistance, self-inductance, and a back-emf. Fig.1 show the BLDC motor is an electronic motor and needs a 3-phase inverter othe driving side for feeding

power into the machine and according to the output from the position sensors inverter works as an electronic commutation which completes the switching of bridge.



Fig.2.1 3-phase Voltage Source Inverter with Motor

2.1 Voltage and Current Control PWM

The current and voltage control operation are essentially two modes of the inverter which are feedback (FB) mode and freewheeling mode. In both these modes switching devices are turned on and off for timing basis to controlled the machine current I_{av} and the machine average voltage V_{av} . In addition to the commutation function controlling the switches in PWM modewe control the voltages and currents continuously at the machine terminal

3.Space Vector Pulse Width Modulation

The space vector concept is used for modifying the inverter output voltage. its derivative from rotating magnetic field theory. the output of inverter can be controlled by using 2-phase Vref component which are drive from 3-phase voltages are transformed either in stationary reference frame or synchronous rotating reference frame in 2-phase voltage.



Fig 3.1: Represent Of Rotating Vector In Complex Plan



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The 3-phase balanced voltages as shown below,

$$V_{as} = V_m \sin \omega t$$
$$V_{bs} = V_m \sin \left(\omega t - \frac{2\pi}{3} \right)$$
$$V_{cs} = V_m \sin \left(\omega t + \frac{2\pi}{3} \right)$$

If In 3- phase BLDC motor we apply the three phase balanced voltage ,rotating flux vector is creates in the air gap of the induction machine rotating with a velocity of ω . Using the Clark's transformation method in stationary reference frame we can calculated this rotating flux vector magnitude and angle as shown below.

$$\vec{V}_{ref} = \vec{V}_{\alpha} + j\vec{V}_{\beta} = \frac{2}{3} \left(V_a + V_b e^{j\frac{2\pi}{3}} + V_c e^{j\frac{4\pi}{3}} \right)$$

Where,

$$\left|V_{ref}\right| = \sqrt{\left(V_{\alpha}^2 + V_{\beta}^2\right)}$$
 and $\alpha = \tan^{-1}\frac{V_{\beta}}{V_{\alpha}}$

Real and imaginary parts is separated using the above equation which are

$$V_{\alpha} = \frac{2}{3} \left(V_{a} \cos 0 + V_{b} \cos \frac{2\pi}{3} + V_{c} \cos \frac{4\pi}{3} \right)$$
$$V_{\beta} = \frac{2}{3} \left(V_{a} \sin 0 + V_{b} \sin \frac{2\pi}{3} + V_{c} \sin \frac{4\pi}{3} \right)$$

The above equations is present in matrix form which are..

$$\begin{bmatrix} V_{\alpha} \\ V_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & \frac{-1}{2} & \frac{-1}{2} \\ 0 & \frac{\sqrt{3}}{2} & \frac{-\sqrt{3}}{2} \end{bmatrix} \begin{bmatrix} V_{as} \\ V_{bs} \\ V_{cs} \end{bmatrix}$$

3.2. Implementation Of Space Vector PWM

In three steps We can implemented SVPWM which are

- 1. Evaluate α , Vd, and Vq.
- 2. Evaluate T0, T1and T2.



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3. Evaluateswitching time of each switching device (S1 TO S6).

3.2.1 Evaluatea andVd , Vq

Using the Clark's transformation 3-phase voltages are transformed to two phase voltages in $\alpha\beta$ stationary reference framethat is shown in figure.3.2

$$V_{d} = \left(V_{a}\cos 0 + V_{b}\cos \frac{2\pi}{3} + V_{c}\cos \frac{4\pi}{3}\right)$$

$$= V_{a} - \frac{1}{2}V_{b} - \frac{1}{2}V_{c}$$
$$V_{q} = \left(V_{a}\sin 0 + V_{b}\sin \frac{2\pi}{3} + V_{c}\sin \frac{4\pi}{3}\right)$$

$$= \frac{\sqrt{3}}{2} V_{b} - \frac{\sqrt{3}}{2} V_{c}$$

$$\begin{bmatrix} V_{d} \\ V_{q} \end{bmatrix} = \begin{bmatrix} 1 & \frac{-1}{2} & \frac{-1}{2} \\ 0 & \frac{\sqrt{3}}{2} & \frac{-\sqrt{3}}{2} \end{bmatrix} \begin{bmatrix} V_{an} \\ V_{bn} \\ V_{cn} \end{bmatrix}$$



Fig 3.2: Reference Vector shown In the Two And Three Dimensional Plane

Where
$$\left|V_{ref}\right| = \sqrt{\left(V_d^2 + V_q^2\right)}$$
 and $\alpha = \tan^{-1}\frac{V_q}{V_d}$

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3.2.2 Calculate T0, T1and T2.

i. CalculateT0,T1 and T2 for sector-1:

In sector-1 the two active voltage vectors and two null vectors are requires to generating a voltage vector Vref at a sampling T_z time. At time T1/Tz interval the active voltage vector V1, at time T2/Tz the active voltage vector V2 are applied, and at a time intervals of T0/Tz and T7/Tz the two null vectors V0 and V7 which are applied respectively.in sector-1 Vref shown in below figure.



Fig 3.3. Calculation VrefIn Sector-1

Calculate Vref Using volt-sec balance equationas follows

$$\frac{1}{T_z} \int_{0}^{T_z} \overline{v}_{ref} dt = \frac{1}{T} \left[\int_{0}^{T_0} \overline{v}_0 dt + \int_{0}^{T_1} \overline{v}_1 dt + \int_{0}^{T_2} \overline{v}_2 dt + \int_{0}^{T_7} \overline{v}_7 dt \right]$$

$$T_{z}\overline{V}_{ref} = T_{1}\overline{V_{1}} + T_{2}\overline{V_{2}}$$

$$\overline{V}_{ref} = \frac{T_1}{T_z} \overline{V_1} + \frac{T_2}{T_z} \overline{V_2}$$

Real and imaginary parts Separate from the above equation, then

$$T_{z} \left| V_{ref} \right| \cos \alpha = \frac{2}{3} V_{dc} T_{1} + \frac{2}{3} V_{dc} T_{2} \cos \frac{\pi}{3}$$
$$T_{z} \left| V_{ref} \right| \sin \alpha = \frac{2}{3} V_{dc} T_{2} \sin \frac{\pi}{3}$$

Tland T2 are calculated using this equations as follows which are



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$$T_{1} = \frac{\left|V_{ref}\right| T_{z} \sin\left(\frac{\pi}{3} - \alpha\right)}{\frac{2}{3} V_{dc} \sin\frac{\pi}{3}}$$
$$T_{2} = \frac{\left|V_{ref}\right| T_{z} \sin\alpha}{\frac{2}{3} V_{dc} \sin\frac{\pi}{3}}$$
$$T_{0} = T_{z} - T_{1} + T_{2}$$

ii. Calculation of T0,T1 and T2 in any sector :

$$T_{z} \left| V_{ref} \right| \begin{bmatrix} \cos \alpha \\ \sin \alpha \end{bmatrix} = T_{1} \frac{2}{3} V_{dc} \begin{bmatrix} \cos (n-1) \frac{\pi}{3} \\ \sin (n-1) \frac{\pi}{3} \end{bmatrix} + T_{2} \frac{2}{3} V_{dc} \begin{bmatrix} \cos \frac{n\pi}{3} \\ \sin \frac{n\pi}{3} \end{bmatrix}$$

Real and imaginary parts Separate from the above equation, then

$$T_{z} \left| V_{ref} \right| \cos \alpha = \frac{2}{3} V_{dc} T_{1} \cos \left(n - 1 \right) \frac{\pi}{3} + \frac{2}{3} V_{dc} T_{2} \cos \frac{n\pi}{3}$$

$$T_{z} \left| V_{ref} \right| \sin \alpha = \frac{2}{3} V_{dc} T_{1} \sin \left(n - 1 \right) \frac{\pi}{3} + \frac{2}{3} V_{dc} T_{2} \sin \frac{n\pi}{3}$$

T1 and T2are calculated Using this equations as follows which are

$$T_{1} = \frac{\sqrt{3}T_{z} \left| V_{ref} \right| \sin\left(\frac{n\pi}{3} - \alpha\right)}{V_{dc}}$$
$$T_{2} = \frac{\sqrt{3}T_{z} \left| V_{ref} \right| \sin\left(\alpha - \frac{(n-1)\pi}{2}\right)}{V_{dc}}$$

 $T_0 = T_z - T_1 - T_2$

n = 1 to 6 (i.e sector 1 to 6) and $0 \le \alpha \le \frac{\pi}{3}$



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3.2.3 Calculate Switching Time Of Each Switching Device (S1 To S6):

For each cycle have a 7 switching states in each sector is shown in table 3.1. The even sector numbers movements in anti-clockwise direction and odd sector numbers movements in clockwise direction.

 $T_{z} = \frac{T_{0}}{4} + \frac{T_{1}}{2} + \frac{T_{2}}{2} + \frac{T_{0}}{4} + \frac{T_{2}}{2} + \frac{T_{1}}{2} + \frac{T_{0}}{4}$

The switching sequence of each sector is shown in Table 3.1

Table 3.1. Switching Times for Each Sector

Sector	Rotor position	Upper switching	Lower switching		
no	in each sector	Devices(S1, S3, S5)	Devices(S4, S6, S2)		
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$		$\begin{split} S_1 &= T_1 + T_2 + \frac{T_0}{2};\\ S_3 &= T_2 + \frac{T_0}{2};\\ S_5 &= \frac{T_0}{2}; \end{split}$	$\begin{split} S_4 &= \frac{T_0}{2} ; \\ S_6 &= T_1 + \frac{T_0}{2} ; \\ S_2 &= T_1 + T_2 + \frac{T_0}{2} ; \\ S_4 &= T_1 + \frac{T_0}{2} ; \\ S_6 &= \frac{T_0}{2} ; \\ S_2 &= T_1 + T_2 + \frac{T_0}{2} ; \end{split}$		
		$\begin{split} S_1 &= T_1 + \frac{T_0}{2};\\ S_3 &= T_1 + T_2 + \frac{T_0}{2};\\ S_5 &= \frac{T_0}{2}; \end{split}$			
3	$120^{\circ} \le \theta \le 180^{\circ}$	$\begin{split} S_1 &= \frac{T_0}{2};\\ S_3 &= T_1 + T_2 + \frac{T_0}{2};\\ S_5 &= T_2 + \frac{T_0}{2}; \end{split}$	$\begin{split} S_4 &= T_1 + T_2 + \frac{T_0}{2} ; \\ S_6 &= \frac{T_0}{2} ; \\ S_2 &= T_1 + \frac{T_0}{2} ; \end{split}$		
4	$180^{\circ} \le \theta \le 240^{\circ}$	$\begin{split} S_1 &= \frac{T_0}{2};\\ S_3 &= T_1 + \frac{T_0}{2};\\ S_5 &= T_1 + T_3 + \frac{T_0}{2}; \end{split}$	$\begin{split} S_4 &= T_1 + T_2 + \frac{T_0}{2} ; \\ S_6 &= T_2 + \frac{T_0}{2} ; \\ S_2 &= \frac{T_0}{2} ; \end{split}$		
5	$240^{\circ} \le \theta \le 300^{\circ}$	$\begin{split} S_1 &= T_2 + \frac{T_0}{2} ; \\ S_3 &= \frac{T_0}{2} ; \\ S_5 &= T_1 + T_2 + \frac{T_0}{2} ; \end{split}$	$\begin{split} S_4 &= T_1 + \frac{T_0}{2} ; \\ S_6 &= T_1 + T_2 + \frac{T_0}{2} ; \\ S_2 &= \frac{T_0}{2} ; \end{split}$		
3	$00^0 \le \theta \le 360^0$	$S_{1} = T_{1} + T_{2} + \frac{T_{0}}{2};$ $S_{3} = \frac{T_{0}}{2};$ $S_{5} = T_{1} + \frac{T_{0}}{2};$	$S_4 = \frac{T_0}{2};$ $S_6 = T_1 + T_2 + \frac{T_0}{2};$ $S_2 = T_2 + \frac{T_0}{2};$		



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IV. CONTROL STRATEGY

4.1 BLDC Motor Current Control Structure

For Hardware implementation of BLDC motor is an advantage of this control technique. This BLDC drive system consists of PM BLDC motor, Space Vector PWM, PI speed controller, Current Transformation, , and an MOSFET inverter are modelled and integrated for simulation in the real-time conditions. The block diagram of BLDC Motor control are shown in fig 4.1.

The BLDCM control system has dual closed-loop control that the outer speed loop and innercurrent loop, and uses classic PI control algorithm. The overall system block diagram is shown in Fig 4.1



Fig 4.1 block diagram of BLDC motor control system

In the current closed loop, Using the coordinate transformation of the electrical system the 3-phase current are converted to the system rotatingco-ordinate current is analysis[6,7] formula as, for the feedback current.

$$\begin{pmatrix} i_{\alpha} \\ i_{\beta} \end{pmatrix} = \sqrt{\frac{2}{3}} \begin{pmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \end{pmatrix} \begin{pmatrix} i_{A} \\ i_{B} \\ i_{C} \end{pmatrix}$$

$$\begin{pmatrix} i_{d} \\ i_{q} \end{pmatrix} = \begin{pmatrix} \cos\theta & \sin\theta \\ -\sin\theta & \cos\theta \end{pmatrix} \begin{pmatrix} i_{\alpha} \\ i_{\beta} \end{pmatrix}$$

Where, *iA*, *iB*, *iC*are phase A,B,C current, *id*, *iq*are d-q coordinate component, *ia*, *iβ* are α - β coordinate component, θ is the axis of the rotor and the stator A phase winding axisangle. Using the motor rotation at the whole simulation system determined the Rotor position. Module of inverter is build by the SVPWM control algorithm and control principle. BLDCMuses Permanent Magnet Synchronous Machine motor module from SIMULINK/SIMPOWERSYSTEMS. Inverter takes general inverter bridge of MOSFET device.

4.2 Structure of Speed Control

For the proper rotation of BLDC motor here use the Electronic commutation circuit, but thespeed of the BLDC motor depends on the voltage amplitude which fed to the motor. For thespeed control of the BLDC motor many PWM techniques are used to control the magnitude of voltage fed to the motor. Various speed controllers are available for thiswe use a PI control system. The error between reference speed and actual speed of the motor is fed input to the controller. Using this error signal the PI controller creates a control signal for the PWM block which changes theON-



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OFF time of the switching devices in the inverter therefore control the voltage fed to the motor. For industrial use PI controller is the best generally used controller because it is easy to implement.

The below equation is defined the structure of speed controller,

$$\mathbf{u}(t) = \mathbf{K}_{e}\left[\mathbf{e}(t) + \frac{1}{T_{I}}\int_{0}^{t}\mathbf{e}(\tau)d\tau\right]$$

Where, e(t) = Reference speed – Actual speed

4.3 Introduction about PI Speed Controller.

The error between the reference valueand the actual value is reduces by the Proportional Integral (PI) controller .DC gain of the system increases by the proportional controller, the steady state error of the system reduces by integral controller . is shown in the Fig 4.2 is show the structure of the PI controller .



Fig. 4.2Closed Loop PI Controller System

Equation of PI controller

$$e(t) = k_p + \frac{k_i}{s}$$

$$e(t) = k_p \left(1 + \frac{1}{T_i s} \right)$$

Where, error e(t) = reference value – actual value

$$T_i = \frac{k_i}{k_p}$$

Where, Ti = constant integral time



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V. MATLAB SIMULATION OF BLDC MOTOR WITH SVPWM



Fig.5.1 Simulation Model Of BLDC drive

Figure 5.1 shows the Simulink model of BLDC Drive. In fig 5.1 show the Subsystem"SVPWM" employs the implementation of space vector PWM and produce the gate pulse of inverter bridge and is shown in figure 5.2.

In fig 5.2 show The block "subsystem1" produce the modulating waveform Tcm1,Tcm2 and Tcm3 is shown in fig 5.3. This modulating signal are generate using the equation which are implement In block "subsystem1".

Insubsystem"produce PWM" the gate pulse for inverter bridge is generate by comparing the modulating signal with high frequency carrier signal. This subsystem are shown in below fig.



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Fig 5.2 Subsystem For Pulse Generation



Fig 5.3 Modulating Signal



Fig.5.4 "produce PWM" subsystem



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Fig.5.5 Signal of Gate Pulse

5.2. Output waveform for variable speed and constant torque of BLDCM

- Fig 5.6 ,5.7, 5.8, 5.9,5.10 and 5.11 shows a set of simulated waveforms for the Three-phase BLDC motor fed through two level inverter.
- The input voltage Vdc=400v carrier frequency fs = 5000Hz
- The speed of motor is change at 2000rpm to 1000rpm and is shown in fig 5.10



Fig.5.6line voltage waveform

			Phase vol	ta pe			
		n					
1	Ψ.						
		1 1 .					
148	0.49	0.5	0.51 0	152 0.	13	M	0.85

Fig.5.7Phase Voltage Waveform



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Fig.5.8 Stator Current Waveform



Fig.5.9Torque Waveform



Fig 5.10Speed Waveform



Fig.5.11Back Emf Waveform



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VI. CONCLUSION

In hardware implementation of industrial area this control technique have wide range of advantages for BLDC motor.

This technique is valid in hardware implementation while using analog to digital converter instead of back EMF zero detector. This paper concludes that, in the current control technique, In this present work, the current control technique are use to control the speed and position of BLDC motor. the error signals of currents achieved are fed to the

rotor reference frame transformation (abc-dq) which develops the d-q currents. Using this d-q currents the d-q voltages are obtained and fed to space vector pulse width modulator which controls the position and speed of BLDC motor. By using MATLAB/SIMULINK the technique is simulated and results derived explain that the torque is controlled efficiently with automatic position and speed control with less harmonics in switching of inverter.

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